

Silicon Photonics for Coherent Applications

C. Doerr

Silicon photonics

SiPh

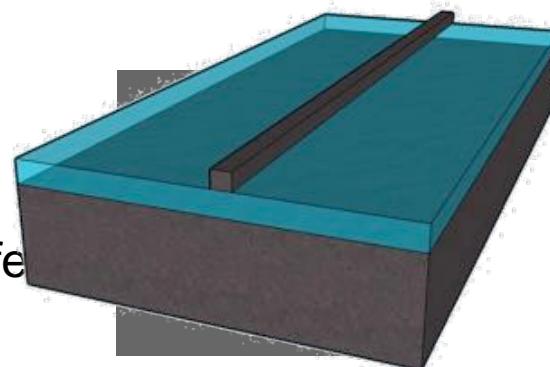


Boule

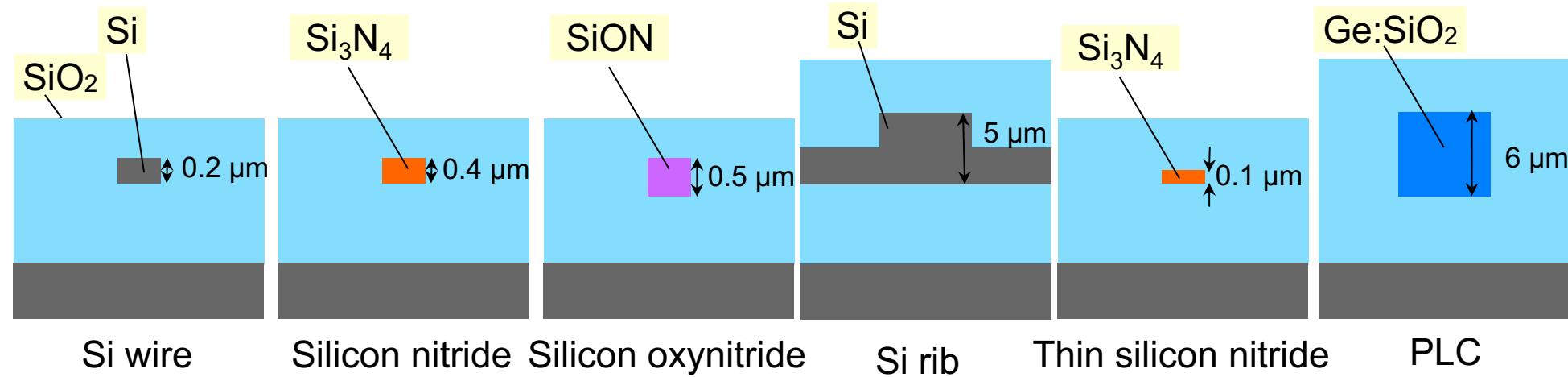


12" (300 mm) wafer

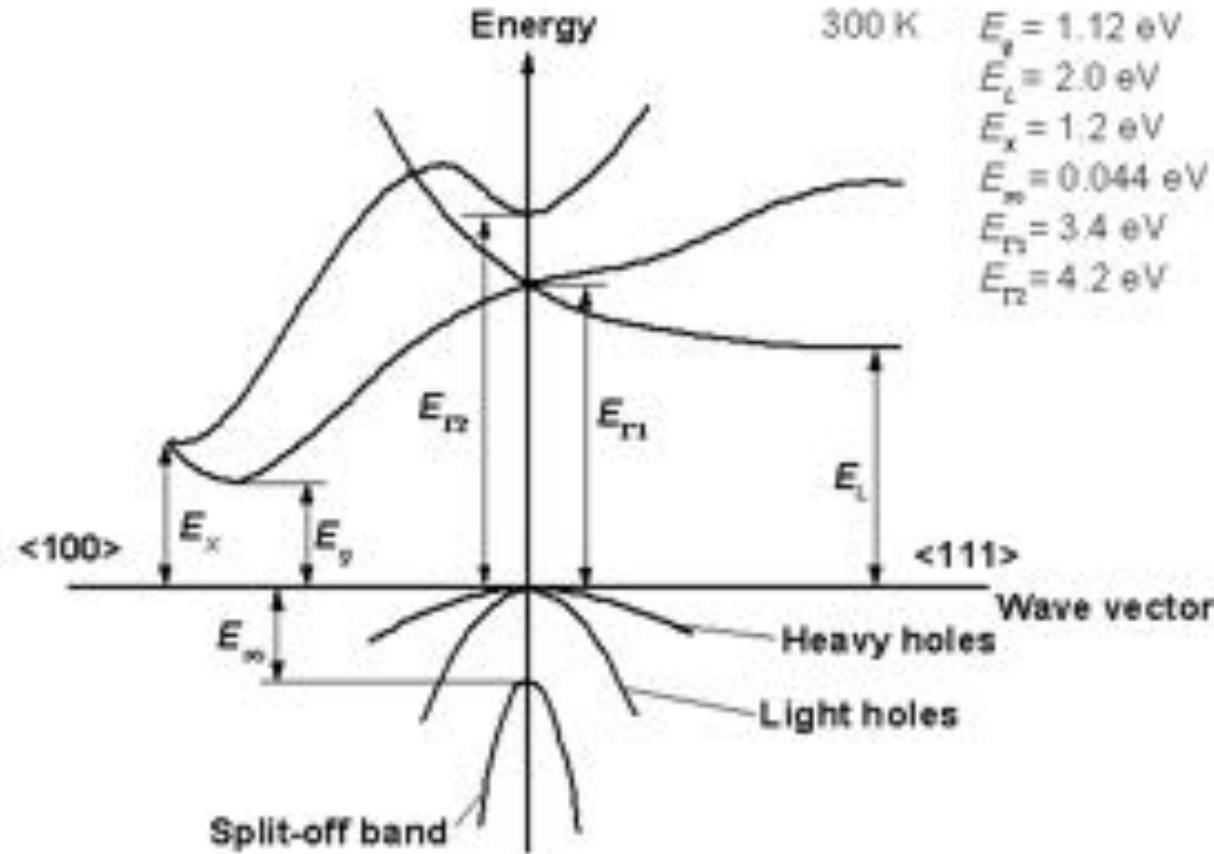
Silicon on insulator (SOI) wafer



SiPh family



Band structure for Si



Electro-refraction/absorption in Si

Refraction

$$\Delta n_r = -8.8 \times 10^{-22} N_e - 8.5 \times 10^{-18} N_h^{0.8}$$

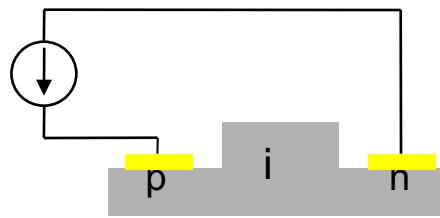
Absorption

$$\Delta n_i = 1.05 \times 10^{-22} N_e + 7.4 \times 10^{-23} N_h$$

N_e = free electron density in cm⁻³

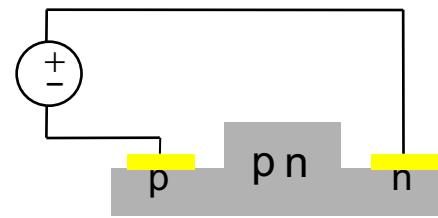
N_h = free hole density in cm⁻³

Electro-optic modulation in Si/Ge



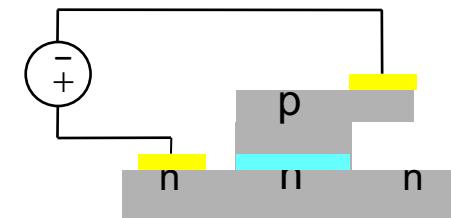
Carrier injection

Causes both phase and magnitude change (can be used as a VOA)
Slow



Carrier depletion

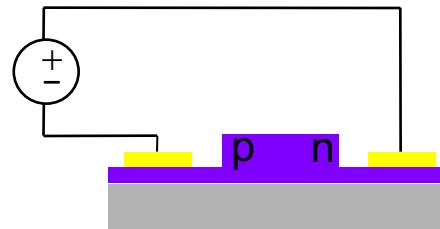
Fast
Weak (typ 2 V-cm)



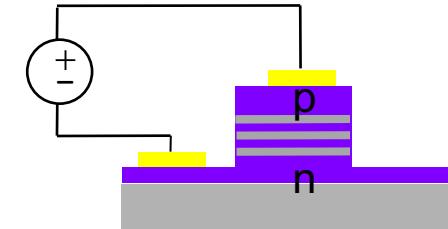
Metal-oxide-semiconductor

Strong (typ 0.2 V-cm)
Fast (but high capacitance)
Lossy

No Pockels effect or QCSE exist in Si

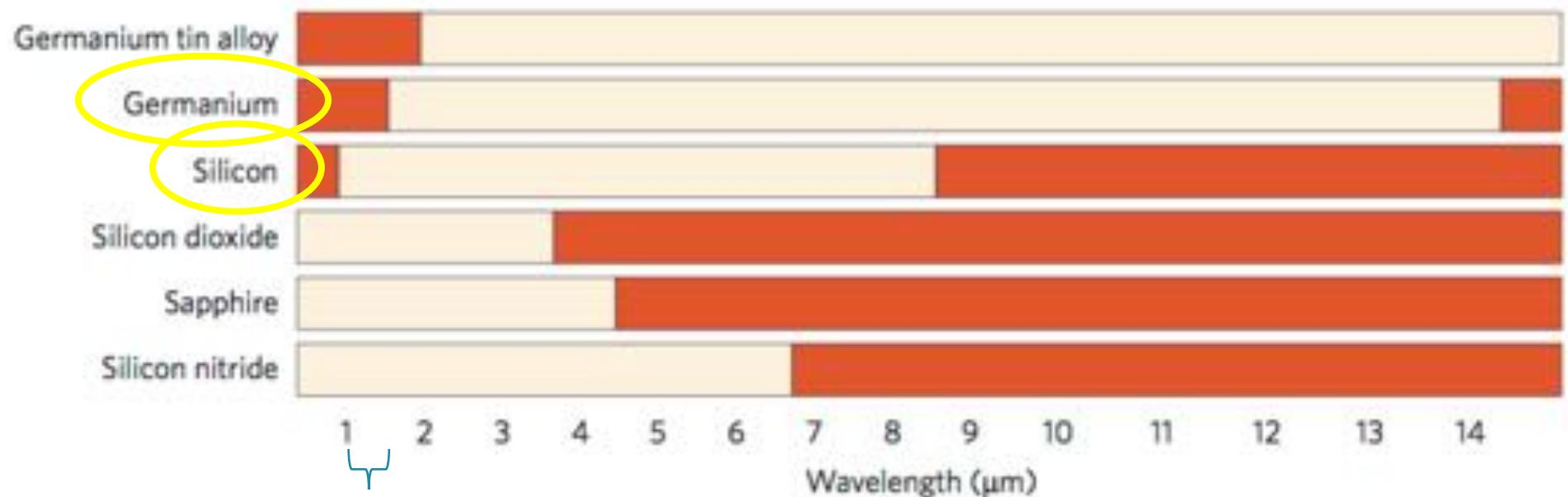


SiGe bulk



SiGe QW

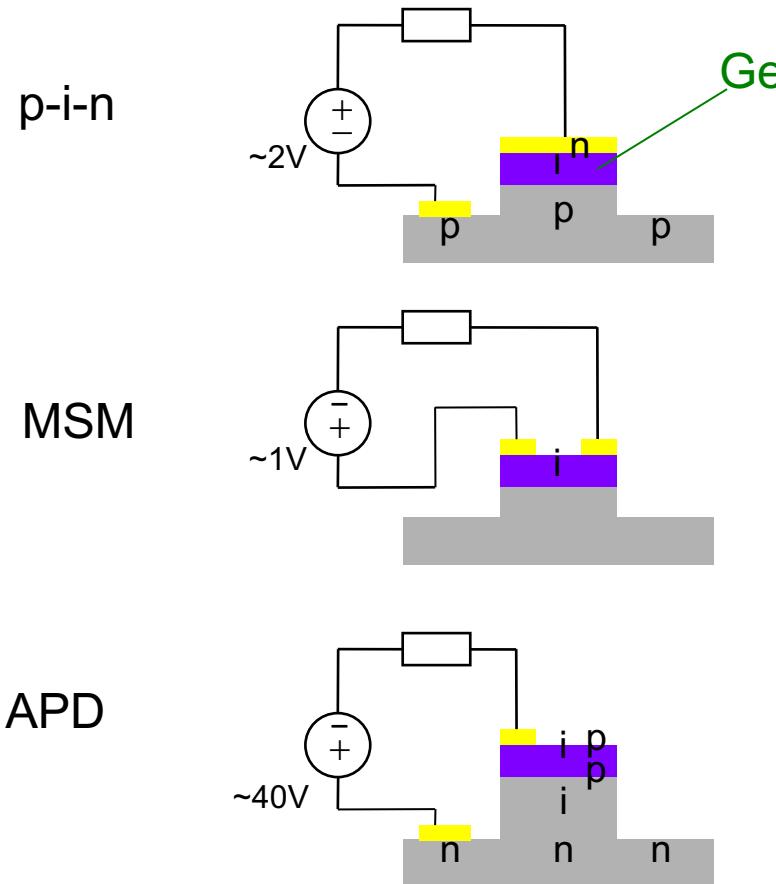
Material transparency



Transmit through Si and receive in Ge

R. Soref, *Nature Photonics*, 2010.

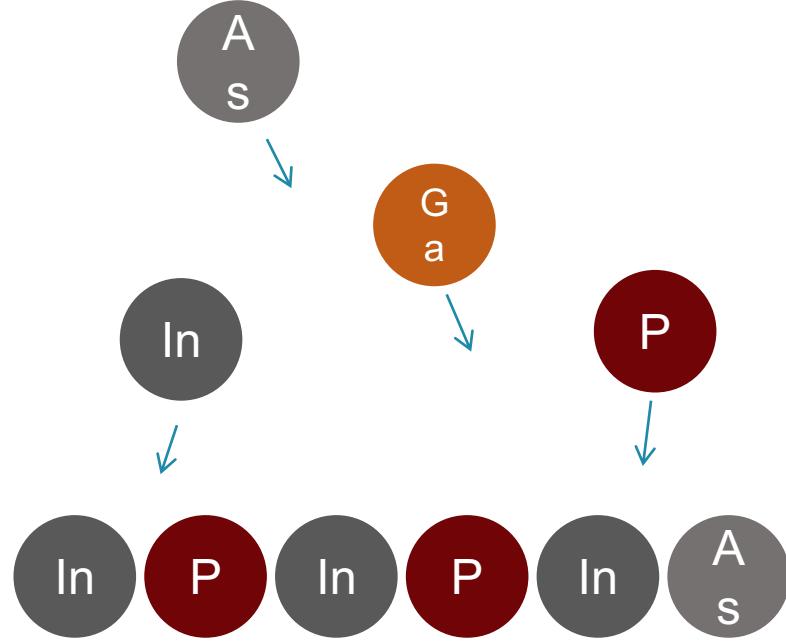
Photodetectors in Si/Ge



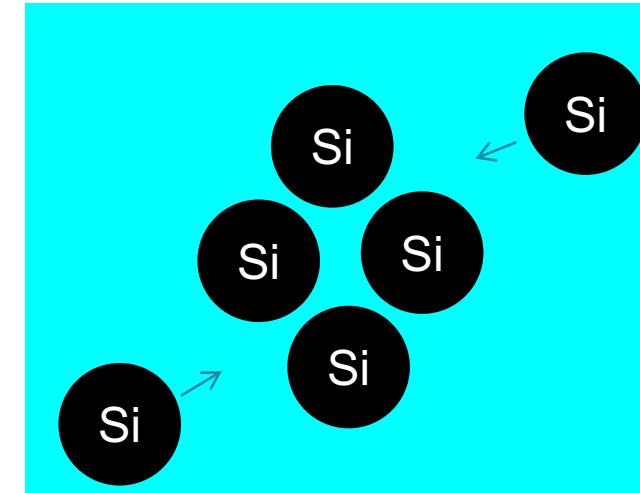
Main advantage of silicon photonics

- Ability to integrate many elements with very high yield
- Not
 - Die cost savings
 - Monolithic CMOS integration

Why SiPh high yield compared to InP?



4 different atom types, dry growth

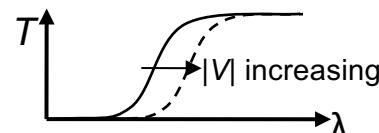
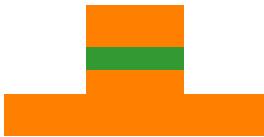


Single atom type, wet growth

InP – SiPh comparison

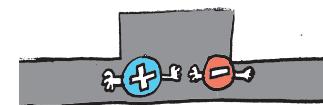
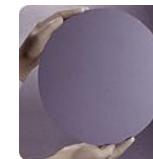
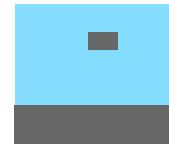
InP

- Expensive material
 - In is scarce
- Medium yield
 - W.g. material from epitaxy
- Small footprint
 - High index contrast in 1D
- Efficient laser
- No good native oxide
- Low dark current
- Small wafers
 - Brittle material
- Modulator temp. sensitive
- Narrow wavelength range
- Not flip-chip-able



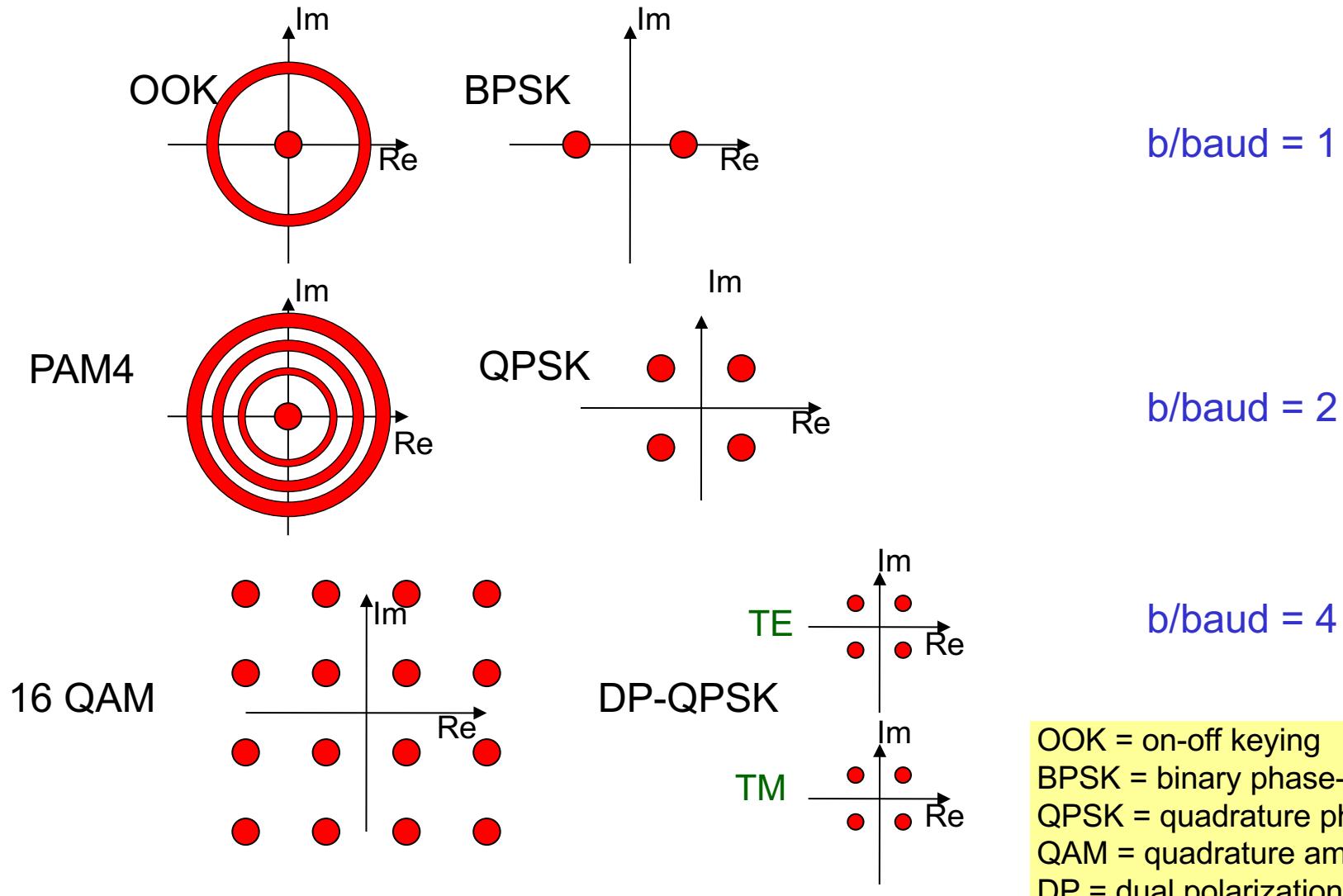
SiPh

- Cheap material
 - 27% Earth's crust is Si
- High yield
 - W.g. material from original boule
- Extremely small footprint
 - High index contrast in 2D
- No native laser
- Excellent native oxide
- Medium dark current
- Large wafers
 - Strong material
- Modulator temp. insens.
- Large wavelength range
- Flip-chip-able



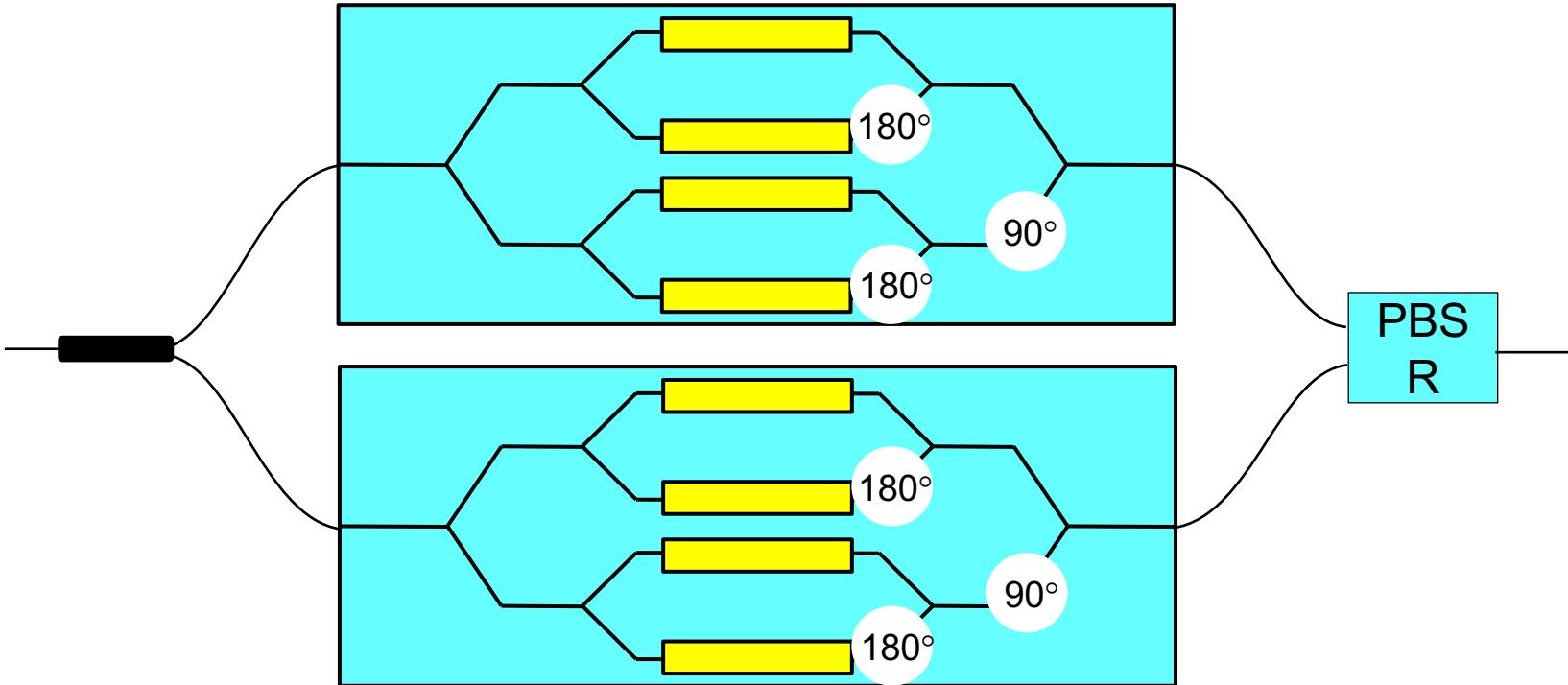
Coherent systems

Advanced modulation formats for optical communication



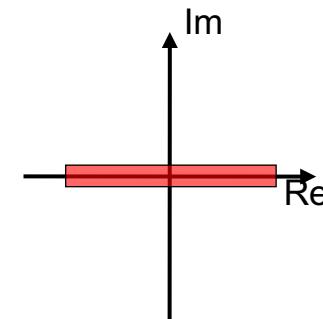
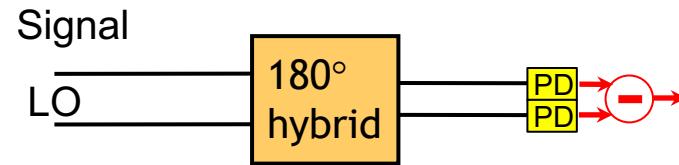
OOK = on-off keying
BPSK = binary phase-shift keying
QPSK = quadrature phase-shift keying
QAM = quadrature amplitude modulation
DP = dual polarization

Advanced modulation format Tx

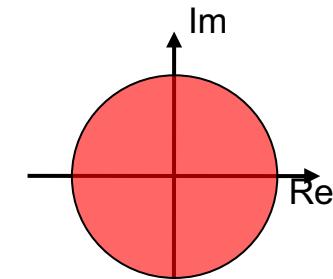
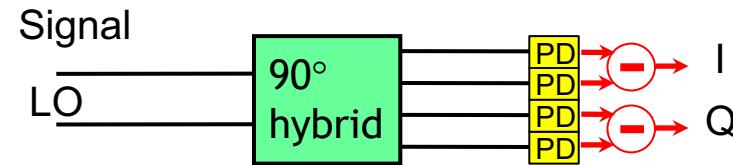


Coherent reception

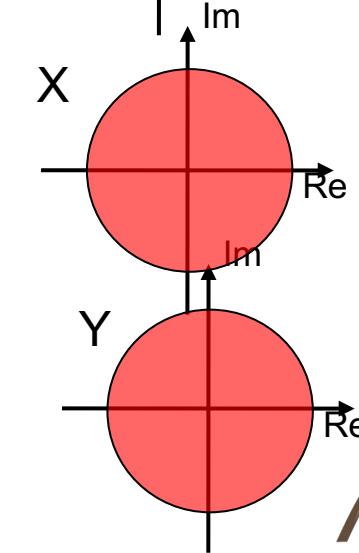
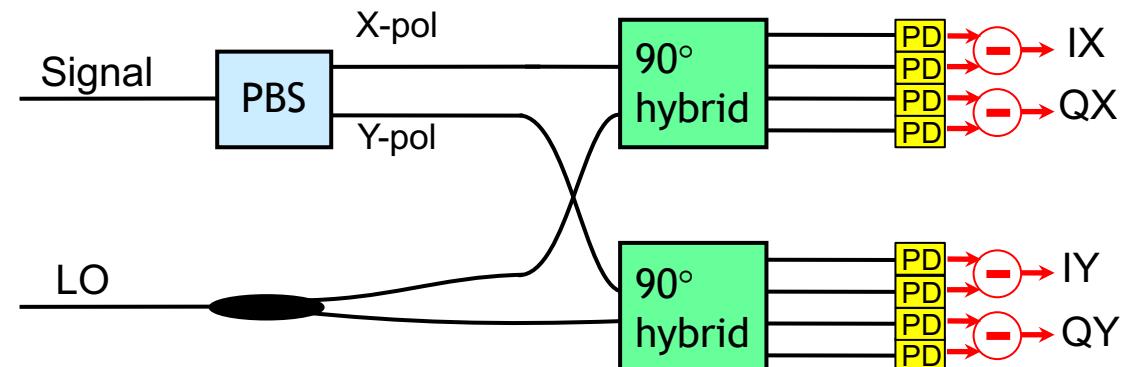
Single quadrature



Dual quadrature



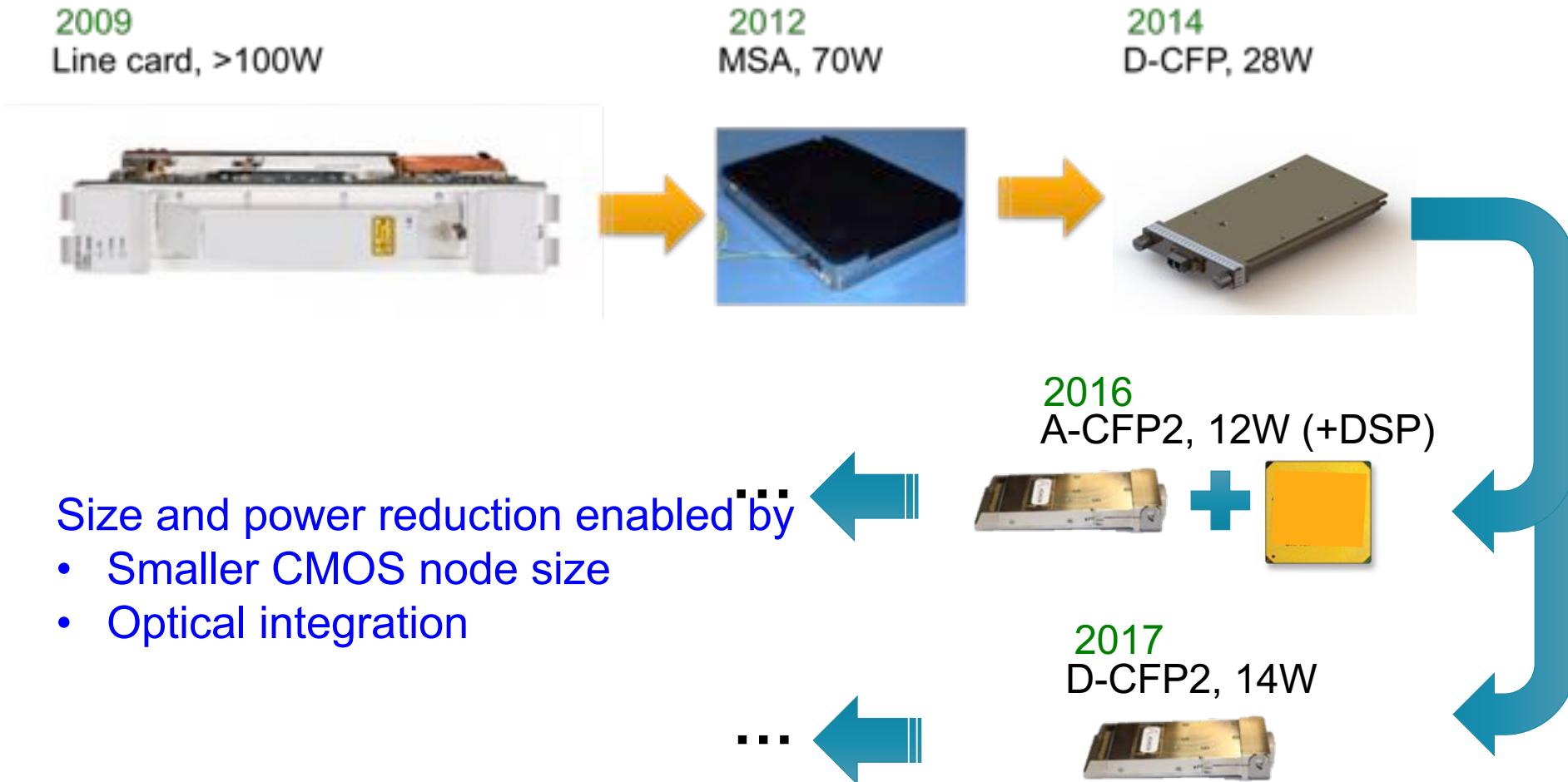
Dual polarization, dual quadrature



Benefits of coherent

- ◆ High spectral efficiency
- ◆ High sensitivity
- ◆ Electronic compensation of impairments
- ◆ No Rx optical filter required
- ◆ Low cost per bit

Coherent module evolution



CMOS node size reduction

Semiconductor manufacturing processes

10 μm – 1971

6 μm – 1974

3 μm – 1977

1.5 μm – 1982

1 μm – 1985

800 nm – 1989

600 nm – 1994

350 nm – 1995

250 nm – 1997

180 nm – 1999

130 nm – 2001

90 nm – 2004

65 nm – 2006

45 nm – 2008

32 nm – 2010

22 nm – 2012

14 nm – 2014

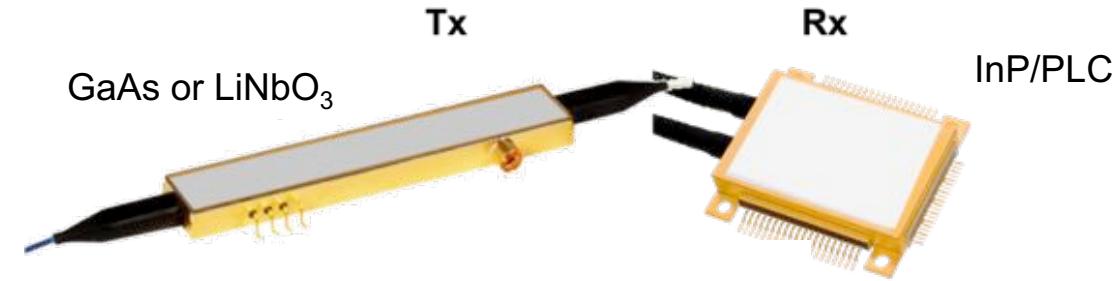
10 nm – 2016

7 nm – 2018

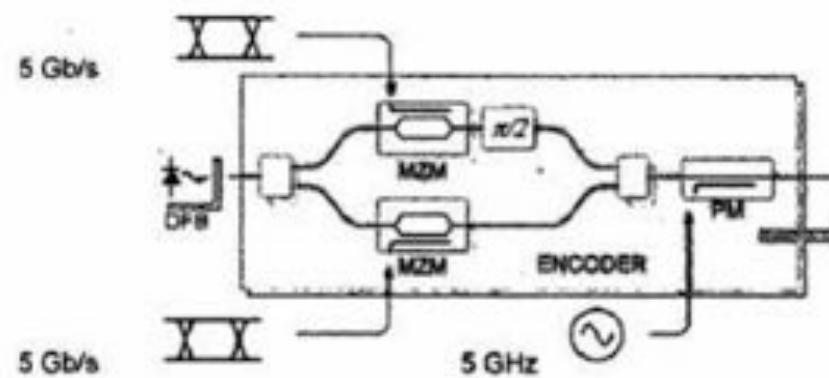
5 nm – 2020

Coherent optics

Coherent optics evolution

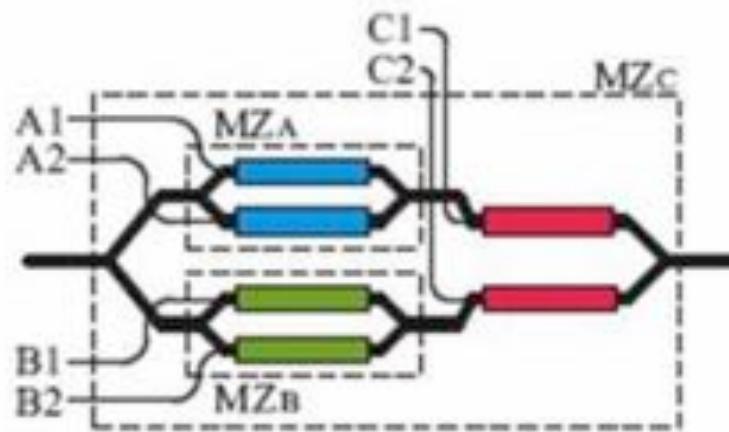


Early advanced format modulators



GaAs

R. Griffin, et al., paper FP6, OFC 2003.



LiNbO₃

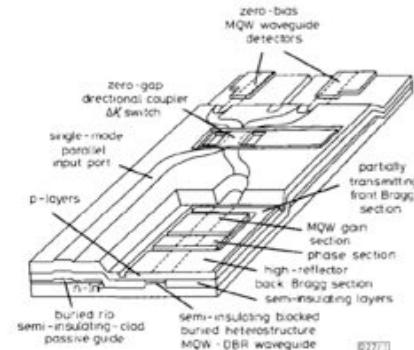
T. Kawanishi, et al., paper OWH5, OFC 2007.

Early coherent receivers

1 pol., 1 quad.

T. L. Koch, et al., Electron. Lett., vol. 25, pp. 1621-1622, 1989.

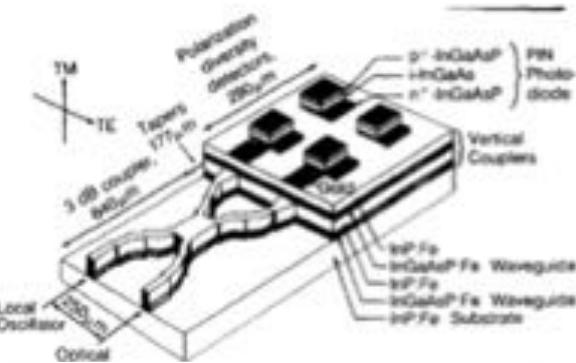
Also, H. Takeuchi, et al., IEEE Photon. Tech. Lett., vol. 1, pp. 398-400, 1989.



InP

2 pol., 1 quad.

R. J. Deri, et al., IEEE Photon. Tech. Lett., p. 1238, 1992.



InP

1 pol., 2 quad.

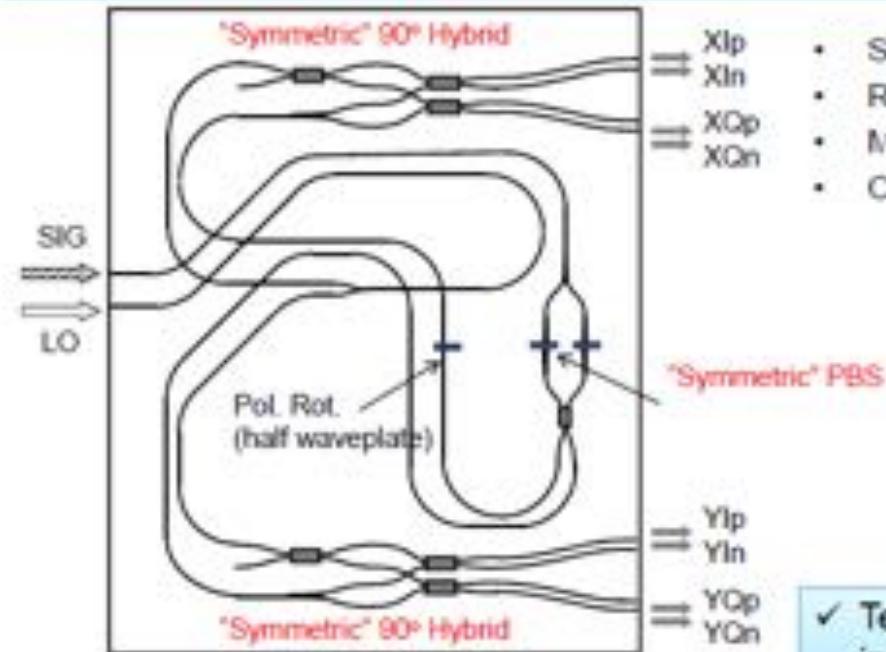
H.-G. Bach, et al., OFC, OMK5, 2009.



InP

PLC coherent receiver

Silica Dual Polarization Optical Hybrid (DPOH)



- Silica on silicon
- Refractive index difference: 1.5 %
- Minimum bending radius: 2 mm
- Chip size: 12.8 x 19 mm

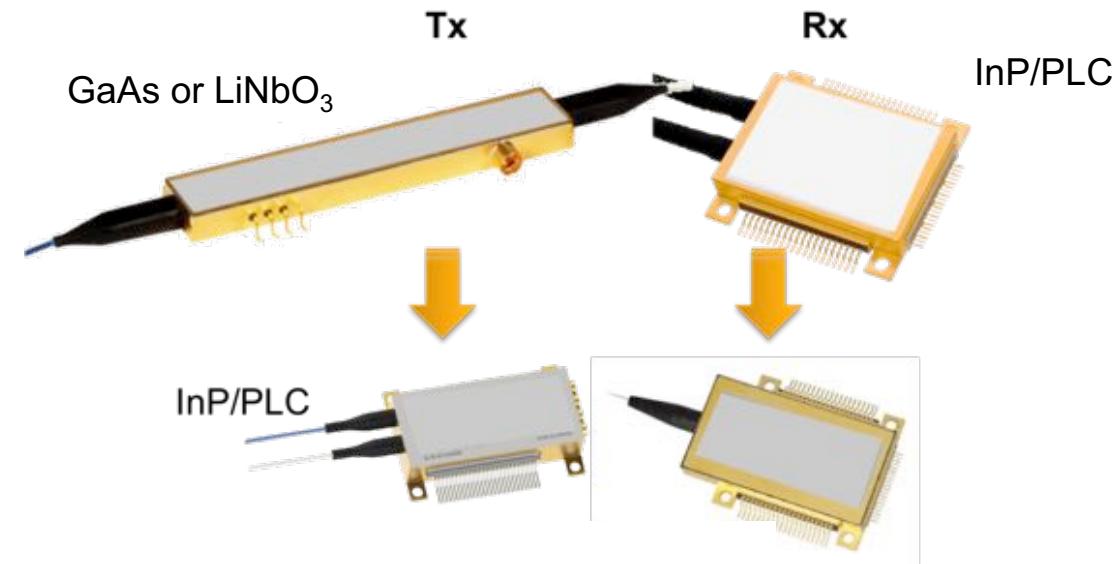
✓ Temperature and wavelength
insensitive dual polarization
optical hybrid

Courtesy of T.
Saida

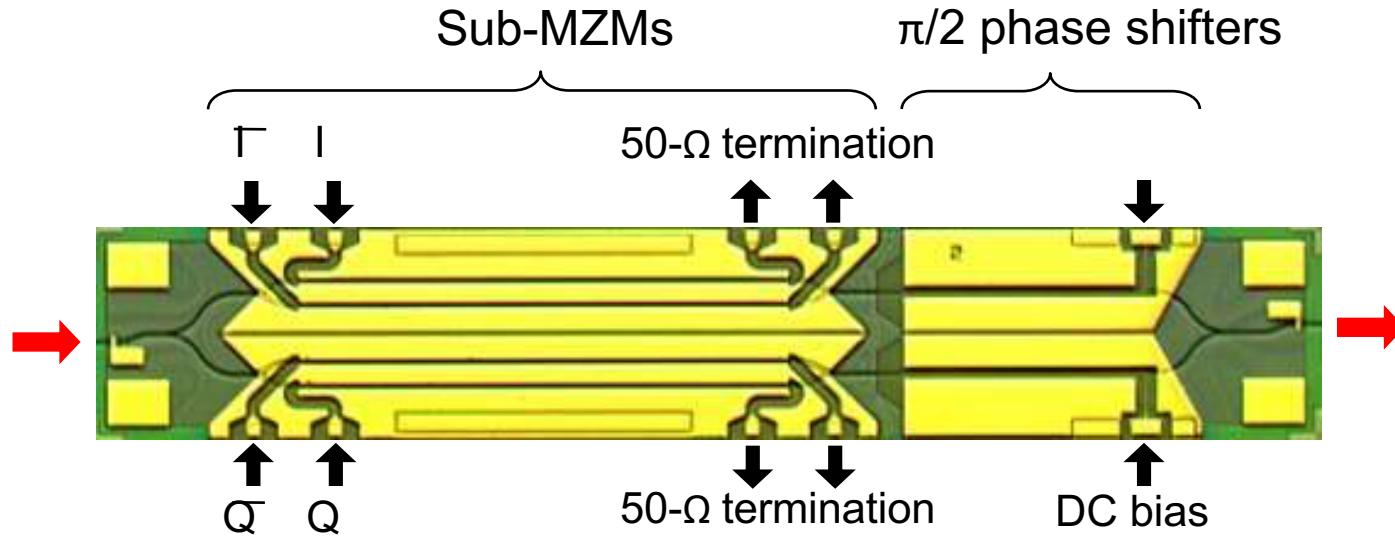


Y. Nasu et al. (NTT), ECOC 2011

Coherent optics evolution

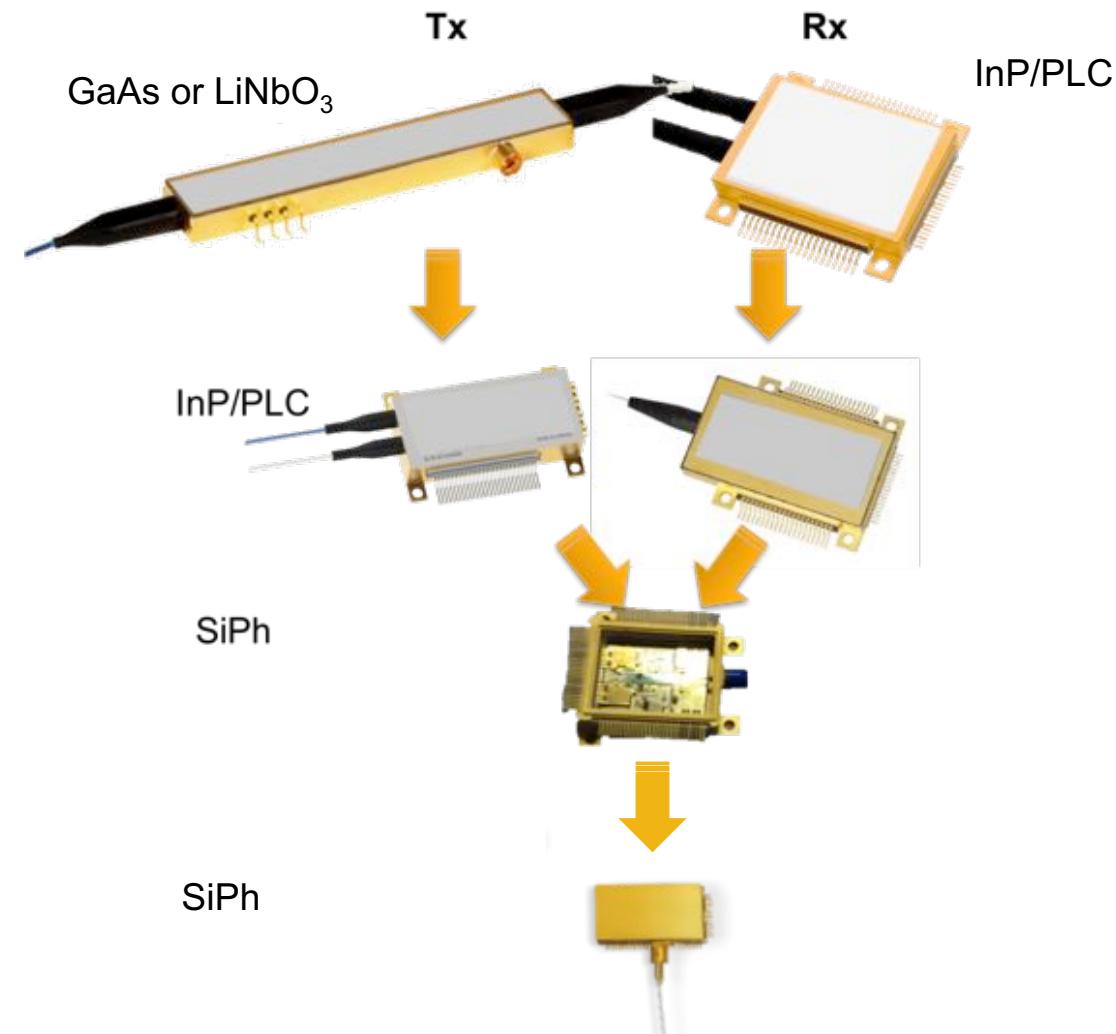


InP advanced format modulator

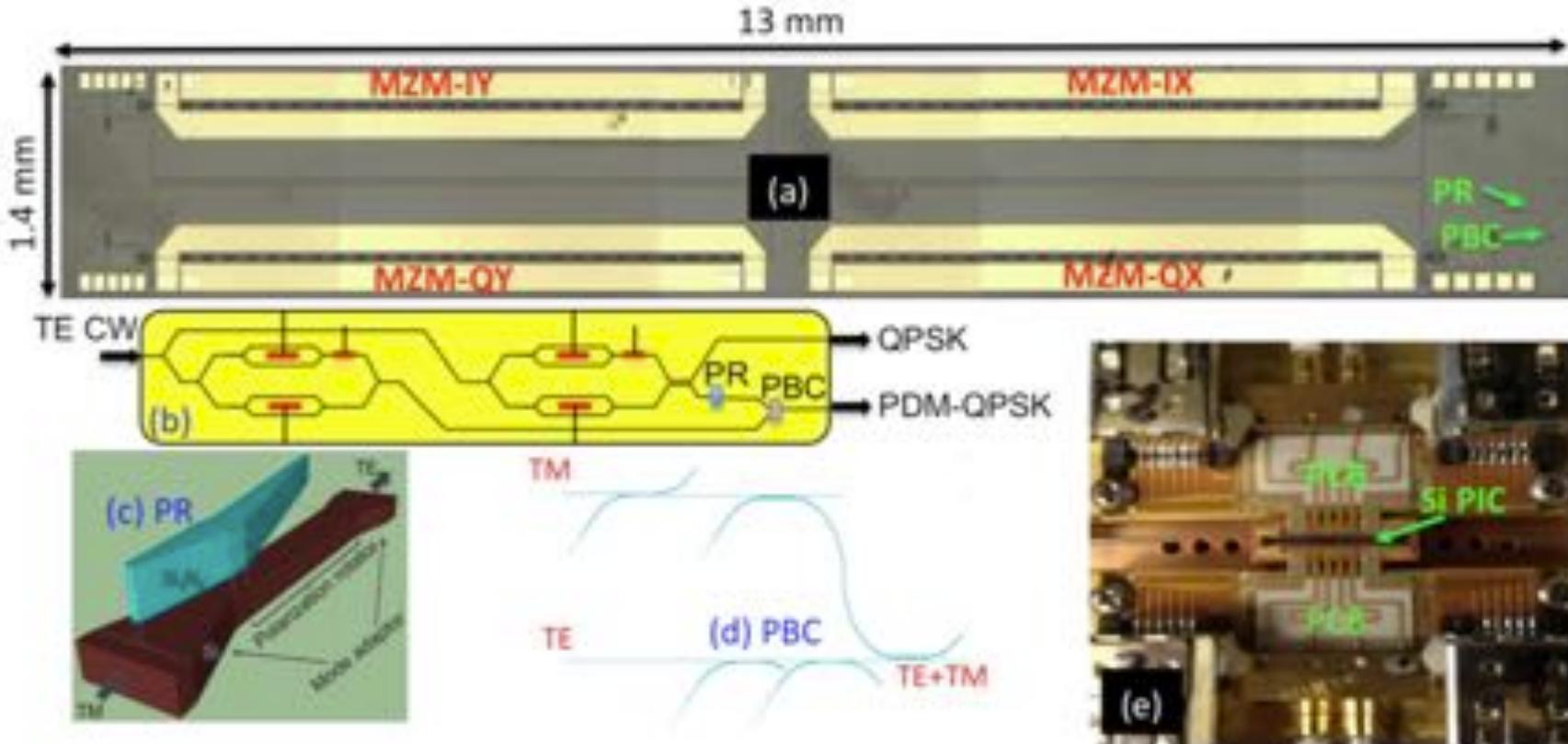


N. Kikuchi, ECOC, 10.3.1, 2007.

Coherent optics evolution

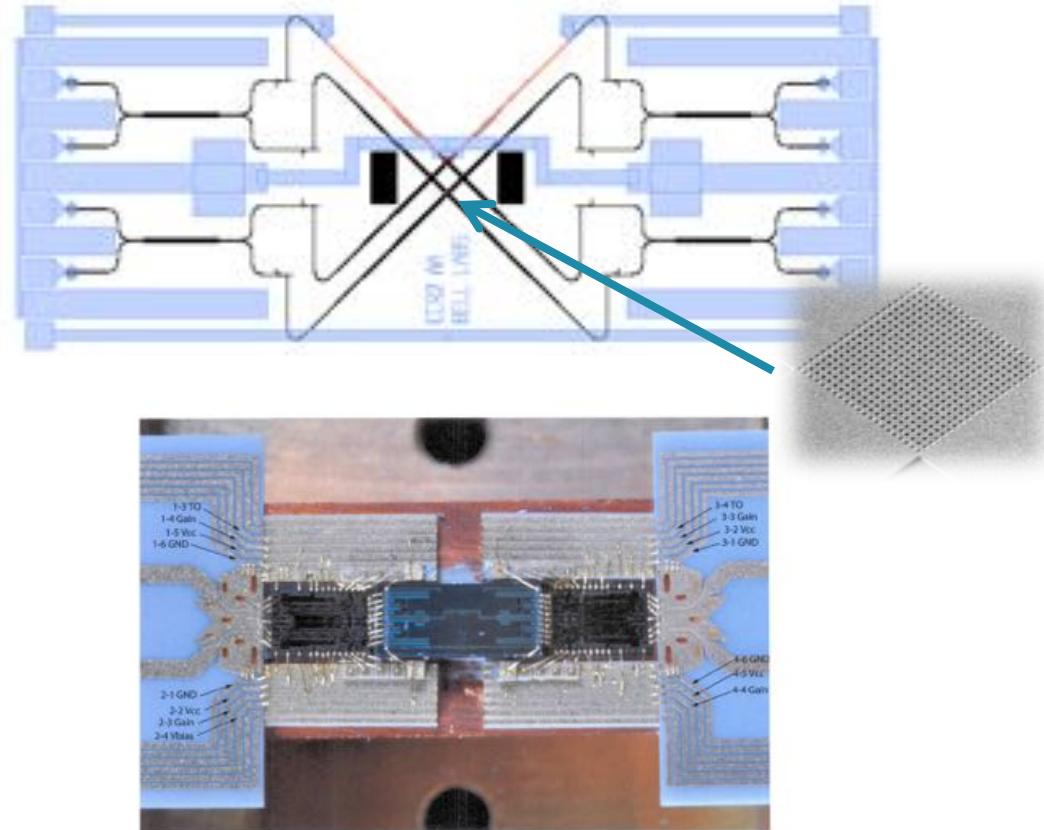


SiPh advanced format modulator



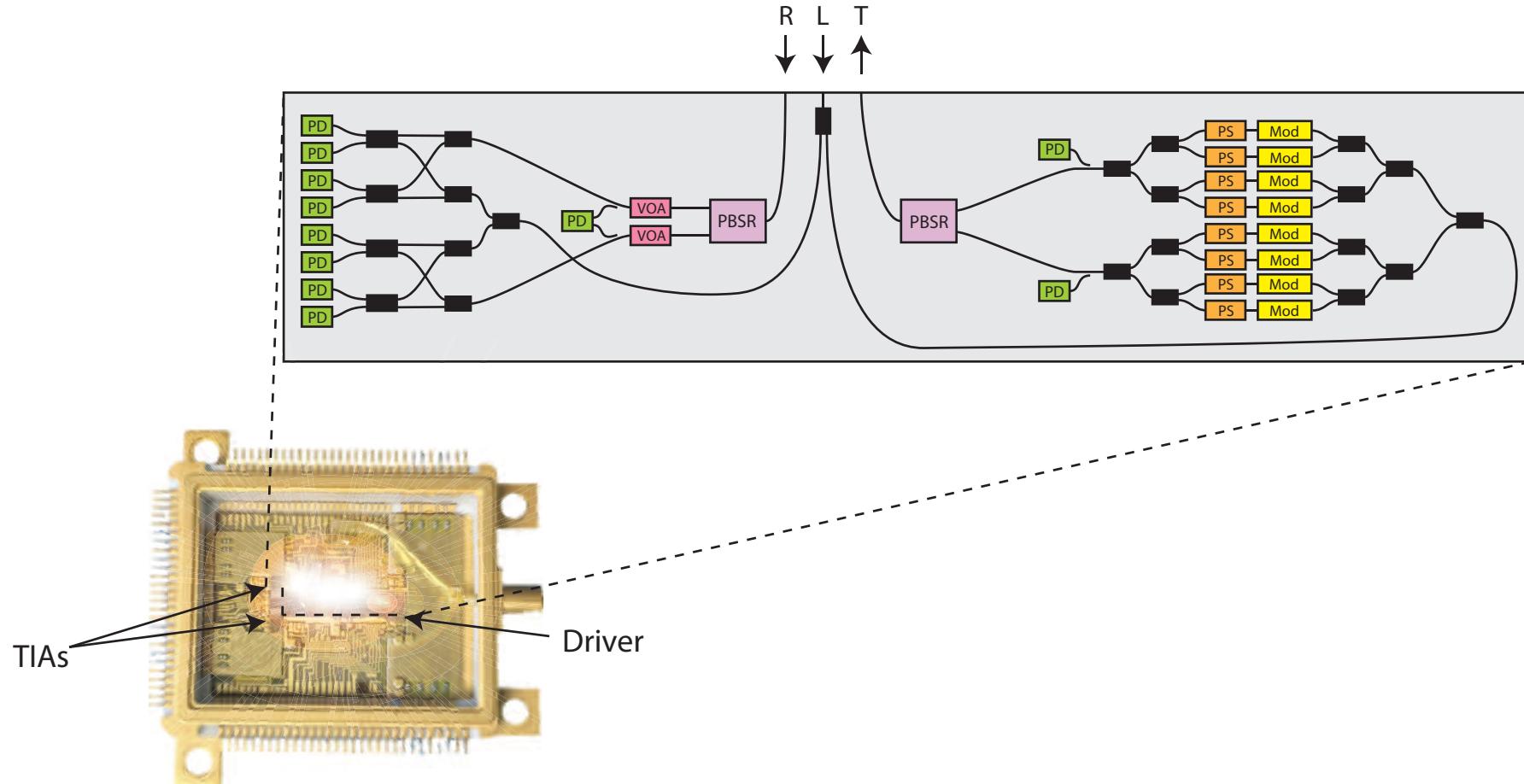
P. Dong, L. Chen, et al., Opt. Exp., 2012.

SiPh coherent receivers



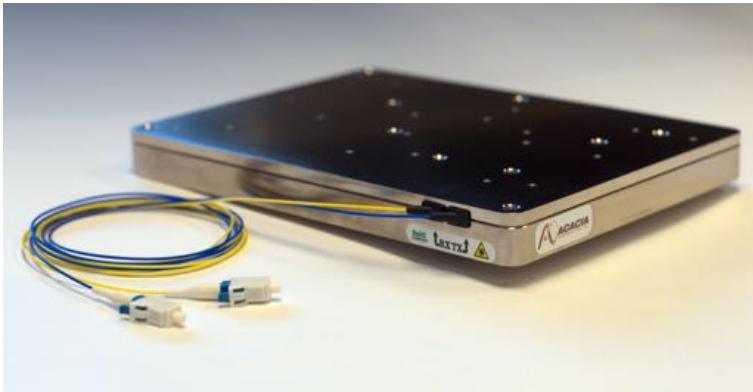
C. R. Doerr, et al., J. Lightwave Tech., vol. 28, pp. 520-525, 2010.
C. R. Doerr, et al., IEEE PTL, 2011.

Single-chip coherent transceiver

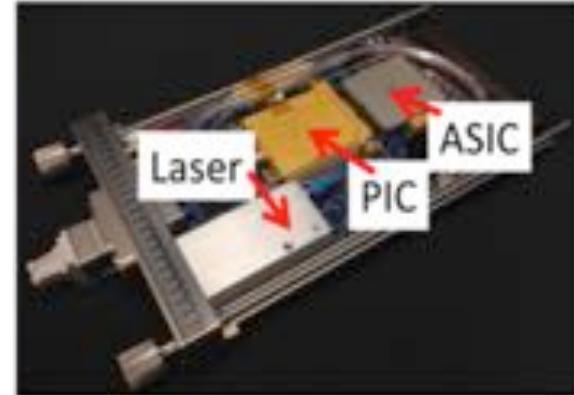


Power consumption = 4.3 W

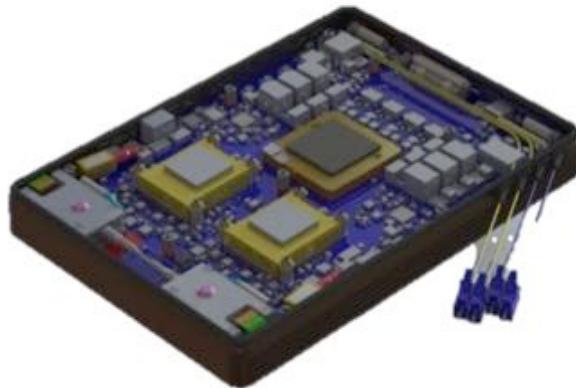
Acacia coherent modules using SiPh



100G MSA



100G CFP



Dual-carrier 400G MSA

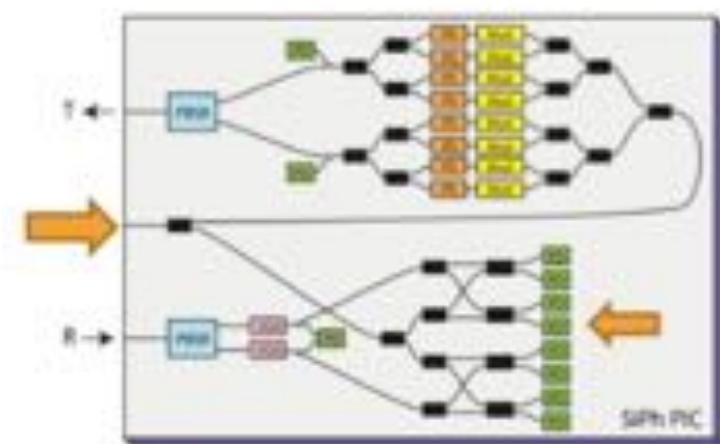


200G CFP2-ACO



200G CFP2-DCO

Example: Rx loss

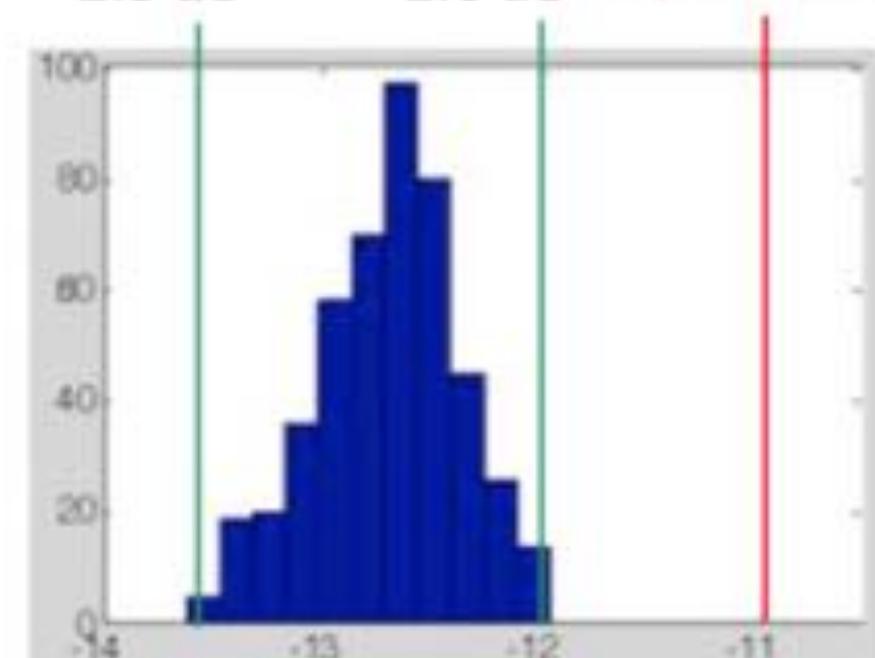


(intrinsic loss: 12 dB)

Equivalent resp: 0.7 A/W
Excess loss: 2.5 dB

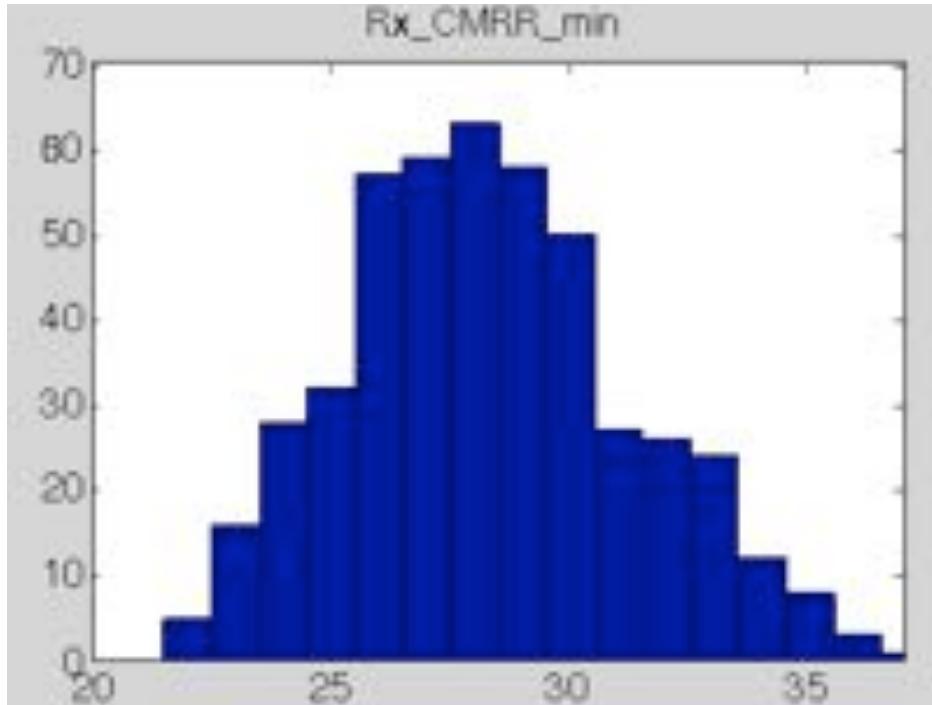
1 A/W
1.0 dB

Theoretical limit:
lossless, 100%
quantum efficiency
(1.25 A/W)



fiber to PD responsivity, A/W in dB

Example: Rx common mode rejection ratio



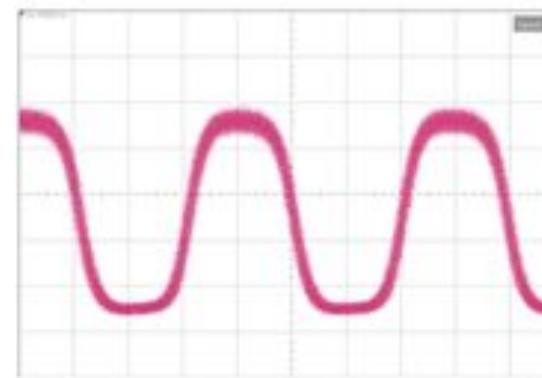
worst Rx CMRR per PIC, in dB scale,
over C-band over 4 pairs of PDs

- CMRR determines the capability for handling multi-channel Rx without demux.
- Mean: 27 dB

Si modulator with linear driver: improved ER and low chirp

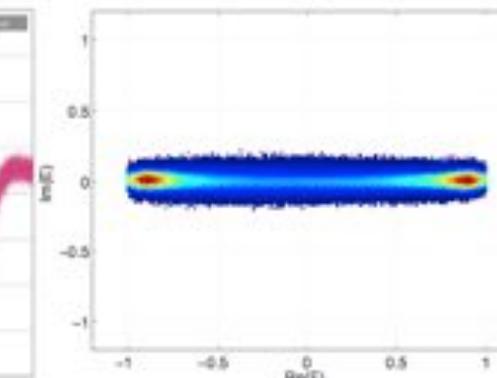
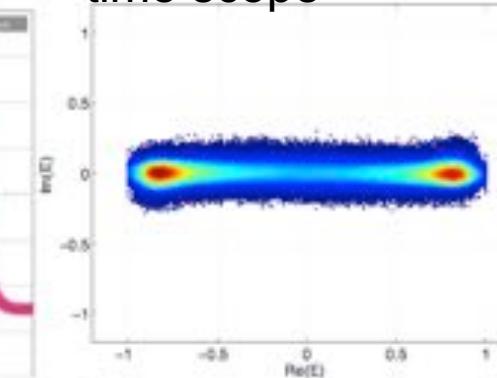
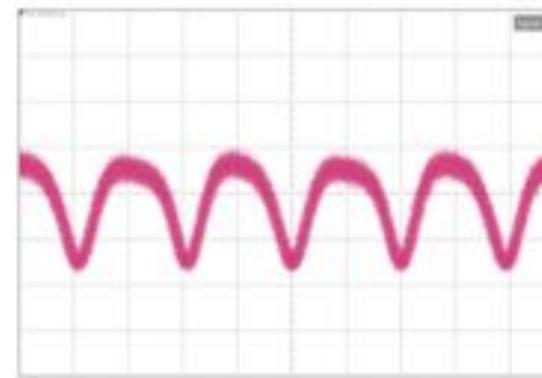
OOK

Waveforms captured
by direct detection
and sampling scope

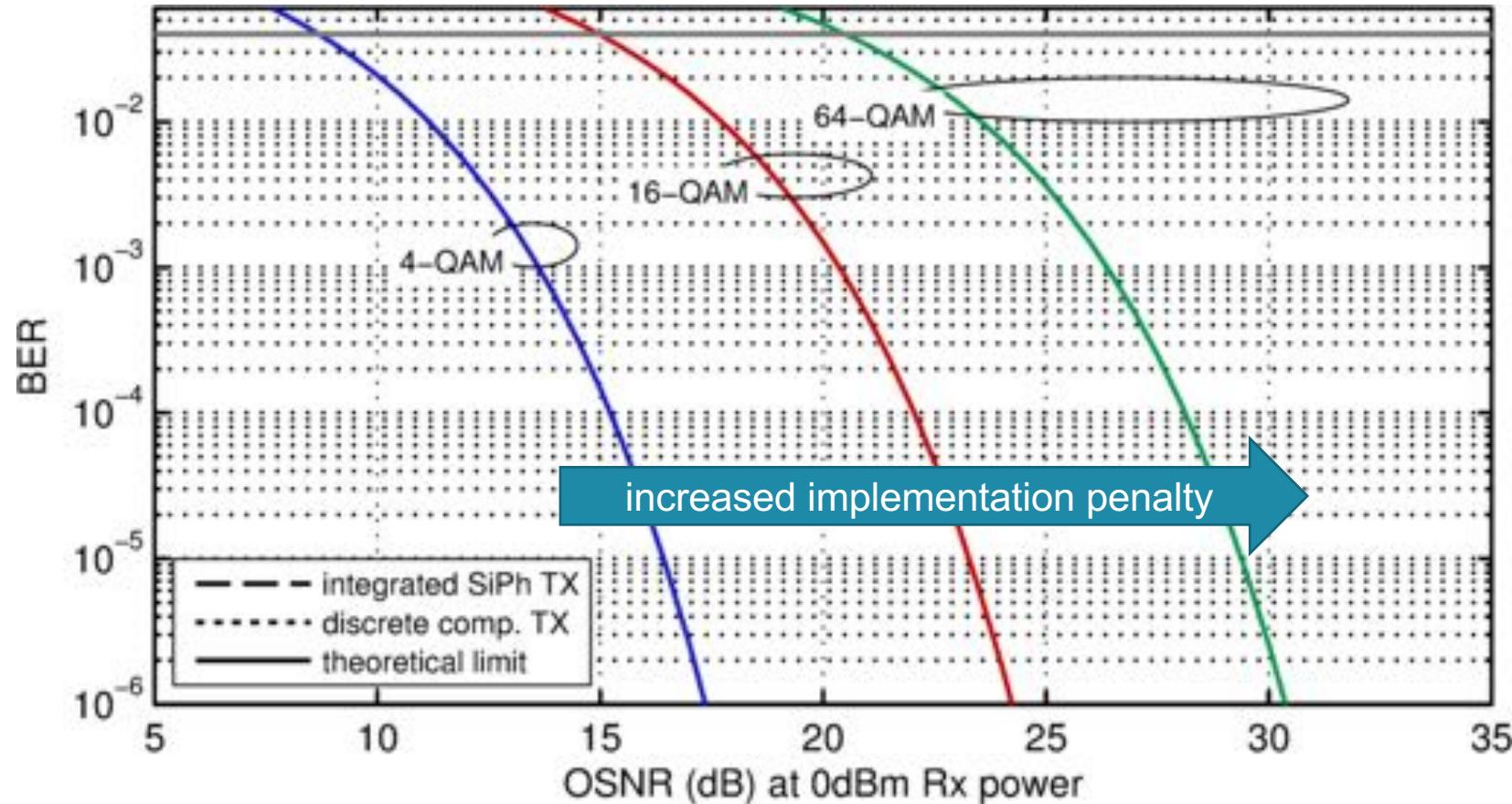


BPSK

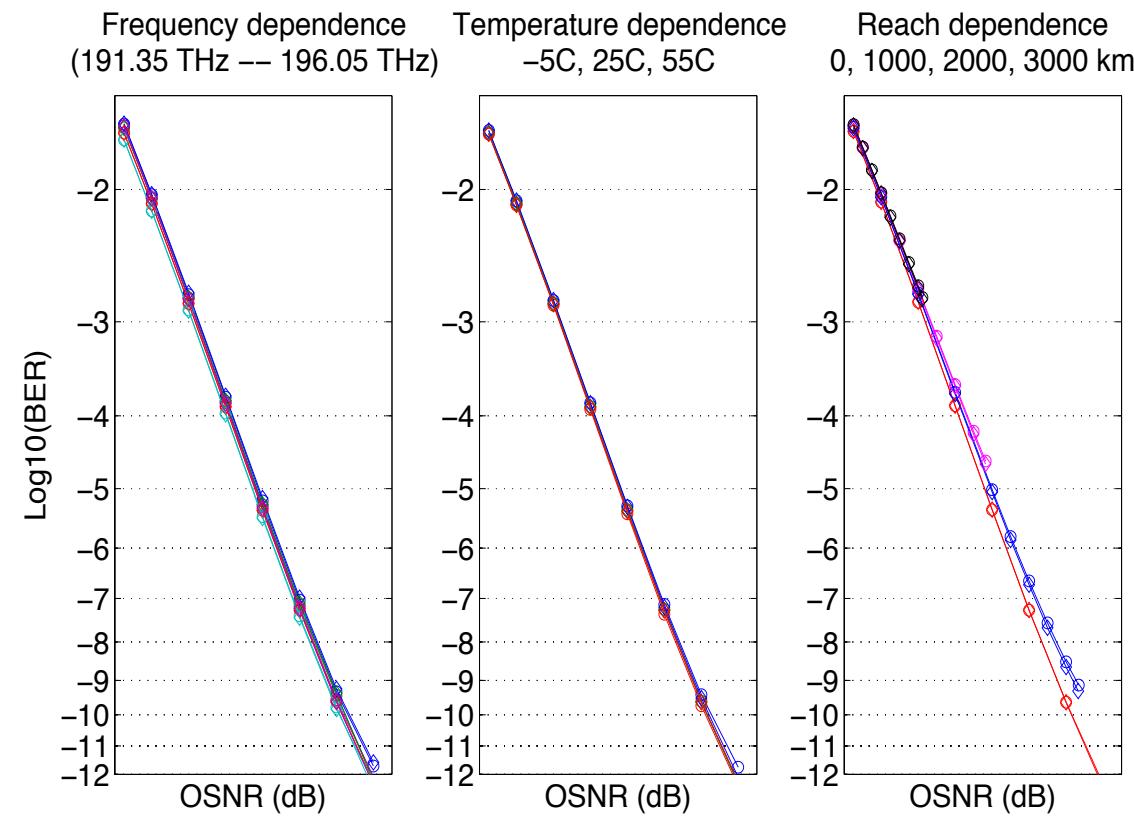
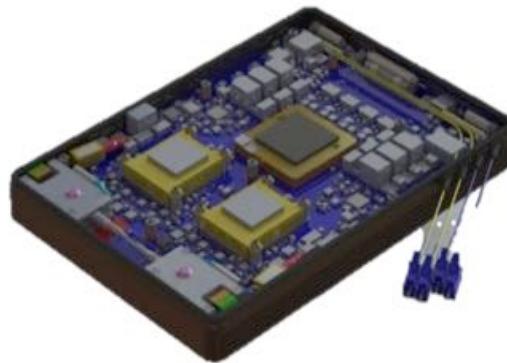
Waveforms captured
by coherent
detection and real-
time scope



Measured performance (30 Gbaud)

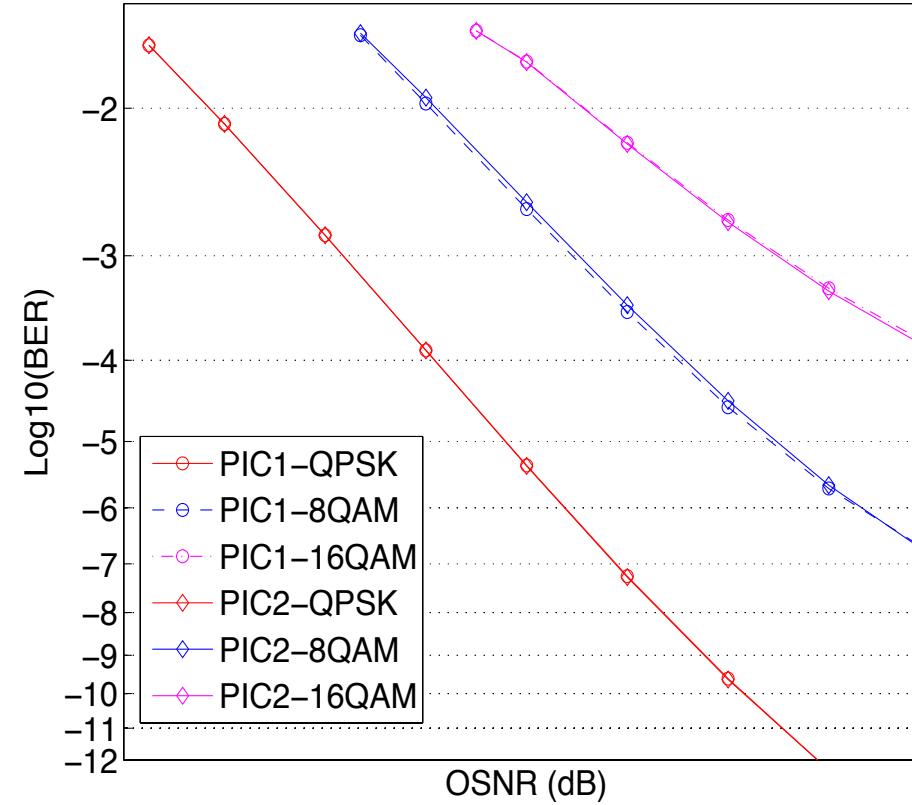
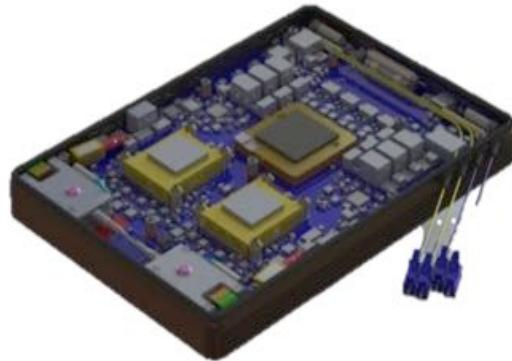


Dual-carrier MSA: wavelength, temperature, and reach at 2 x 100G



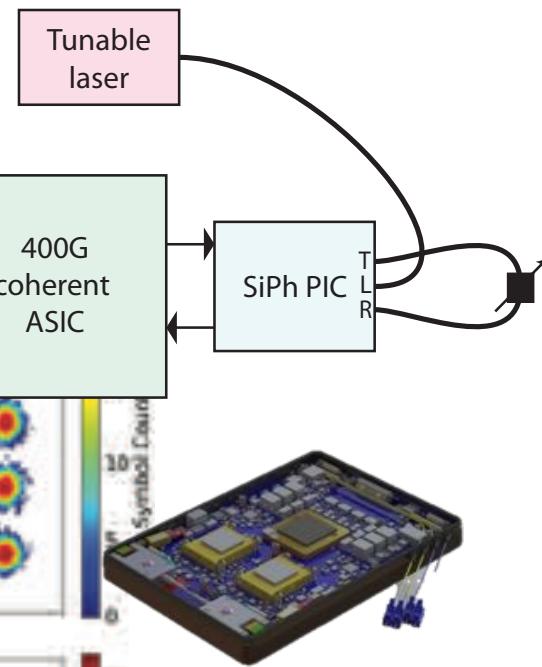
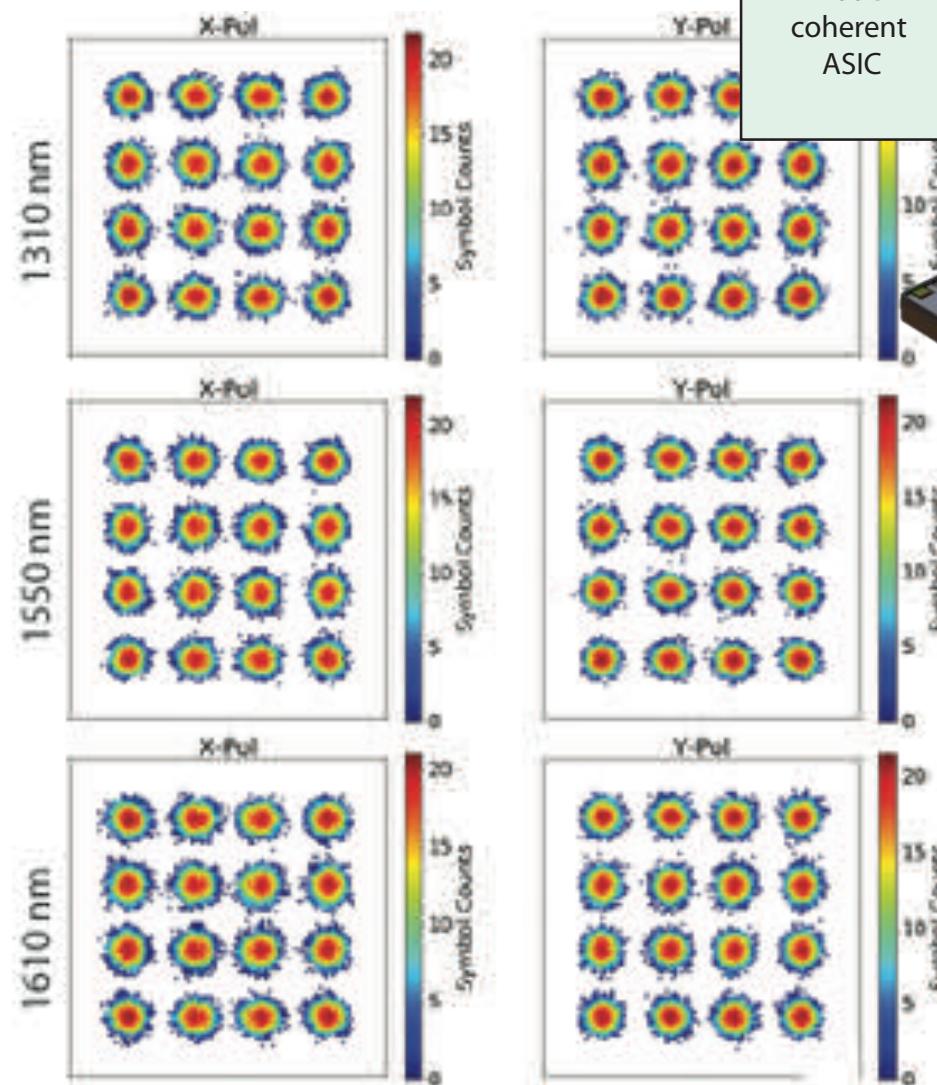
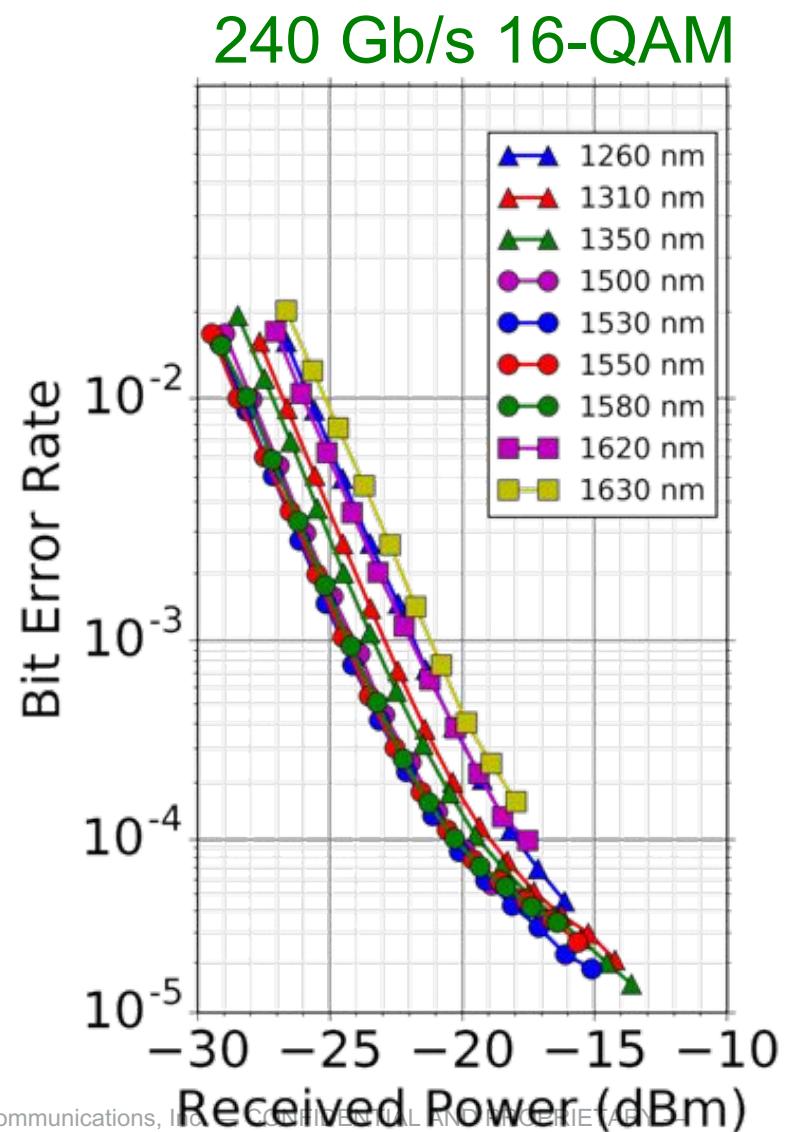
Results of two lanes are super-imposed.

Dual-carrier MSA: variable data rate of 2x100G, 2x150G, 2x200G

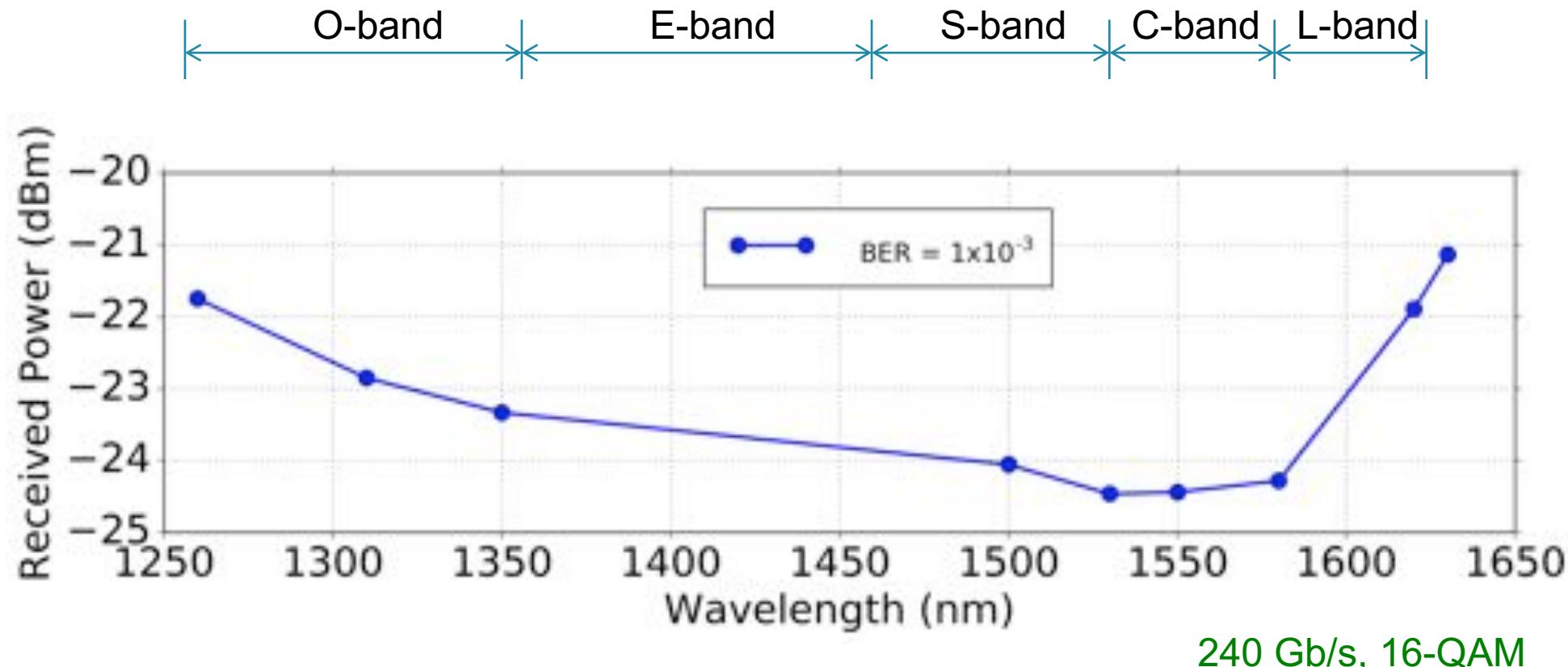


Results of two lanes are super-imposed.

370-nm bandwidth demonstration



Received power at 10^{-3} BER

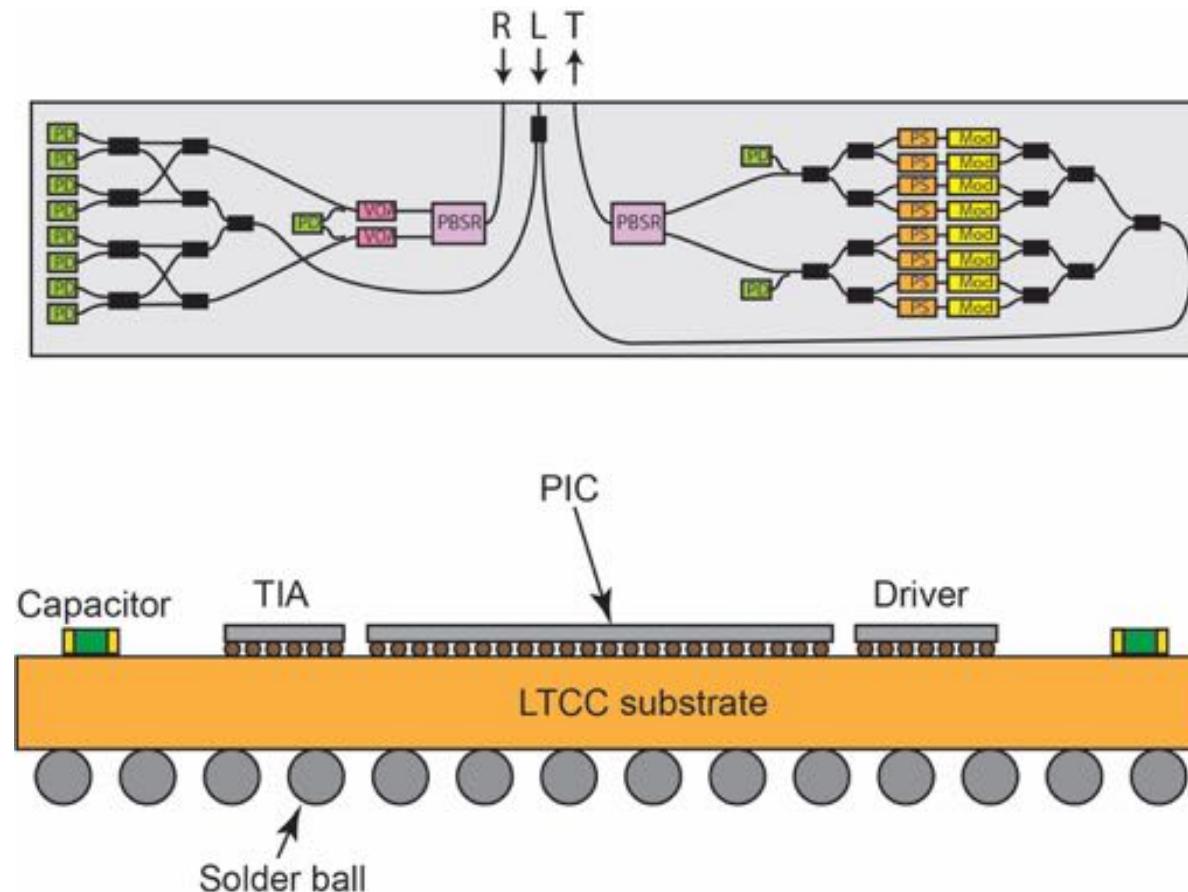


Tx loss variation = 3.7 dB

Rx loss variation = 3.5 dB

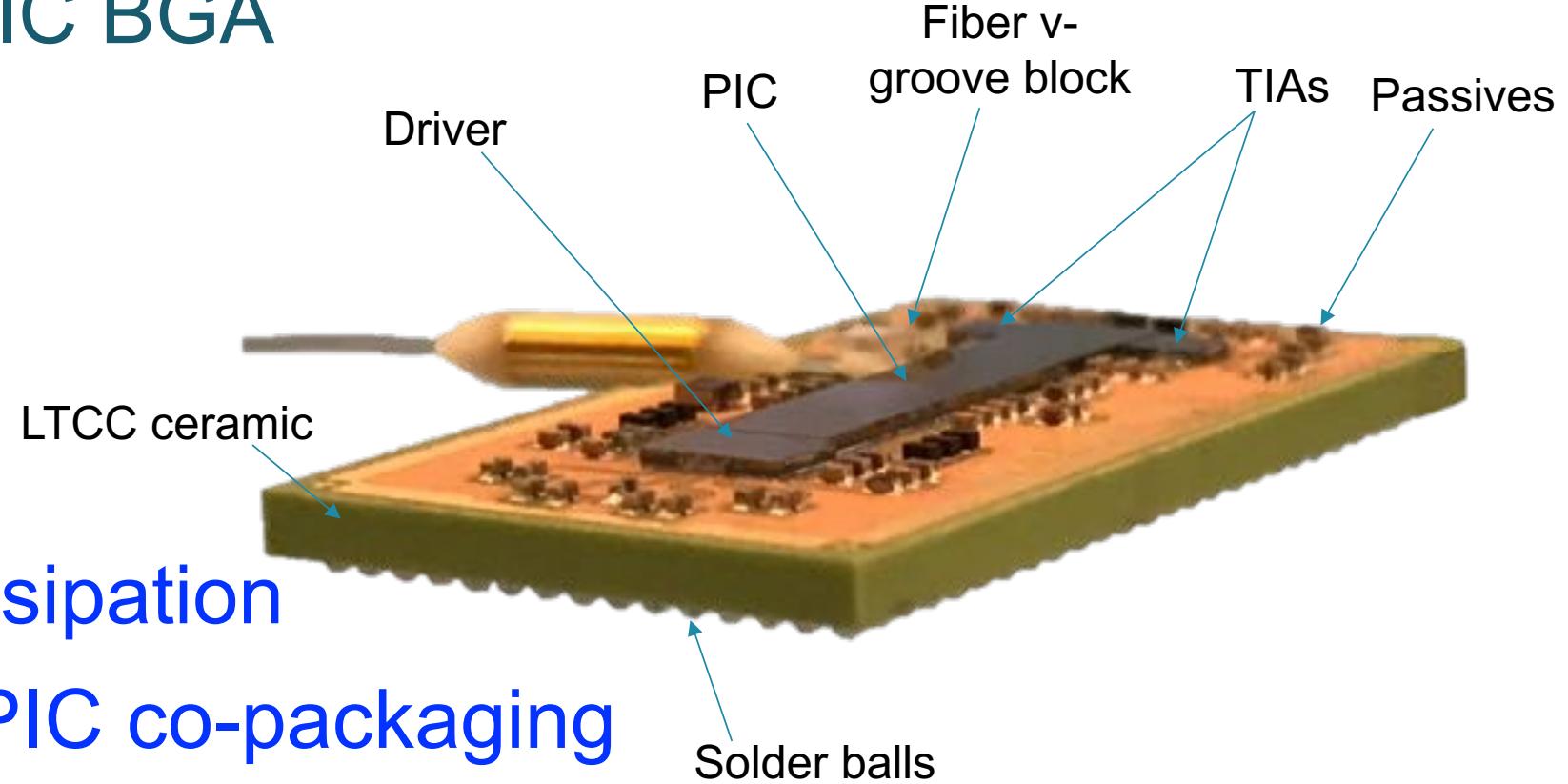
Reduced cost packaging

BGA schematic



Advantages of PIC BGA

- Lower cost
- Higher speed
- Smaller footprint
- Improved heat dissipation
- Leads to ASIC + PIC co-packaging



21.6mm x 13.0mm
369 balls, 0.8-mm pitch
3.5mm height with lid

Lower cost

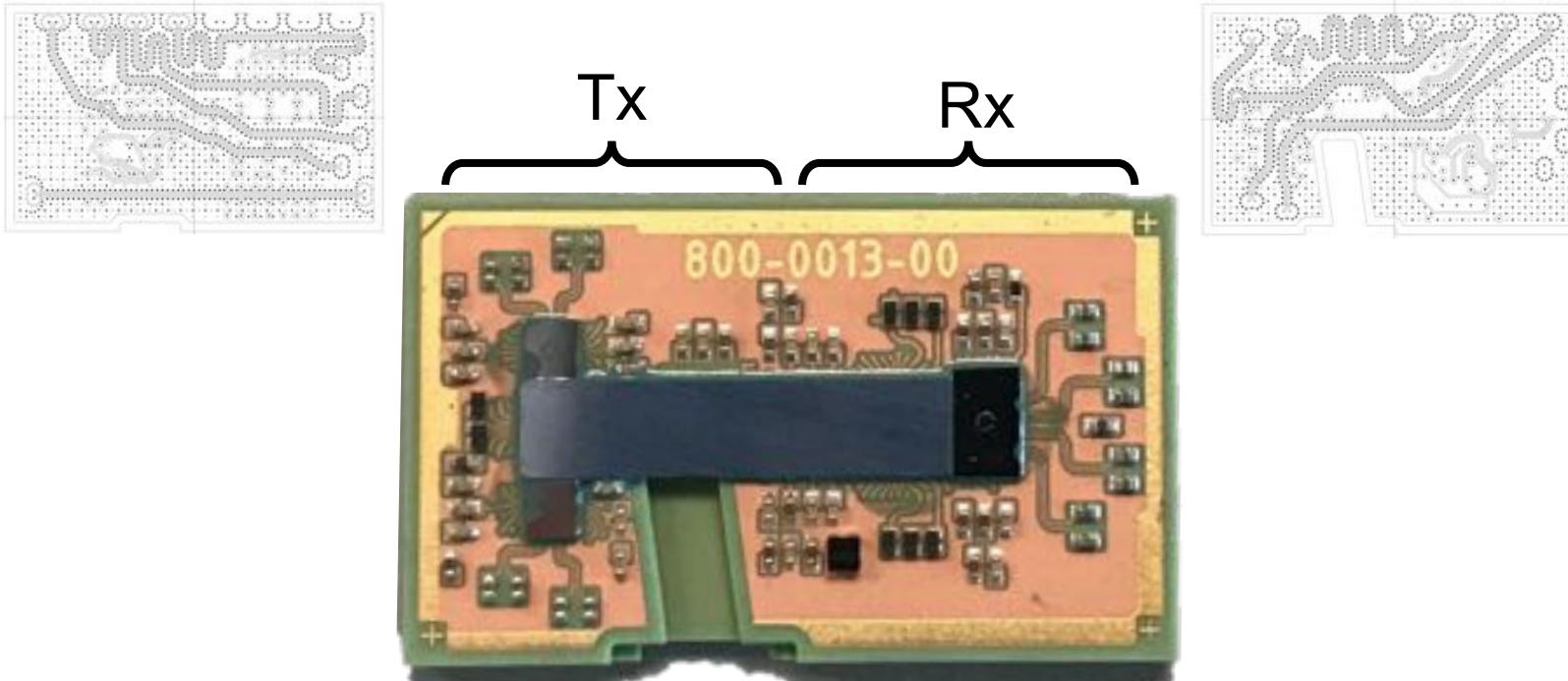
- Package
 - Single-step manufacturing process
 - Fewer parts
 - Basically a small PCB
- Assembly of package
 - Automated passives placement
 - Automated die bonding
- Assembly into module
 - Treated as regular SMT component

Higher speed

- No wire bonds
- Copper, rather than tungsten, traces

Smaller footprint

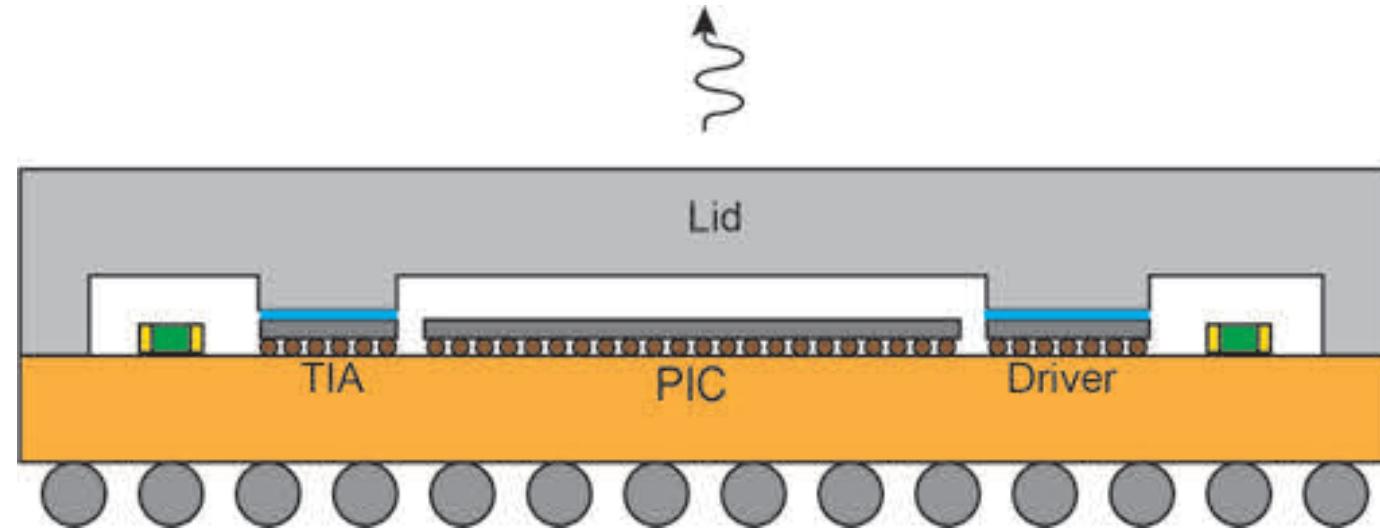
- No package pins
- Smaller footprint for both package and PCB traces



Routing to match ASIC is done inside substrate, so PCB traces can be very short

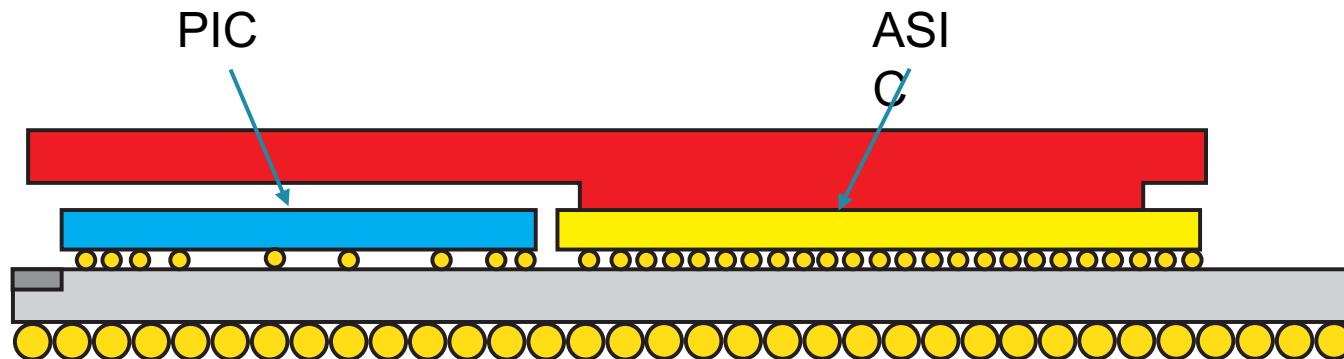
Improved heat dissipation

- Heat flows directly from die backside to lid

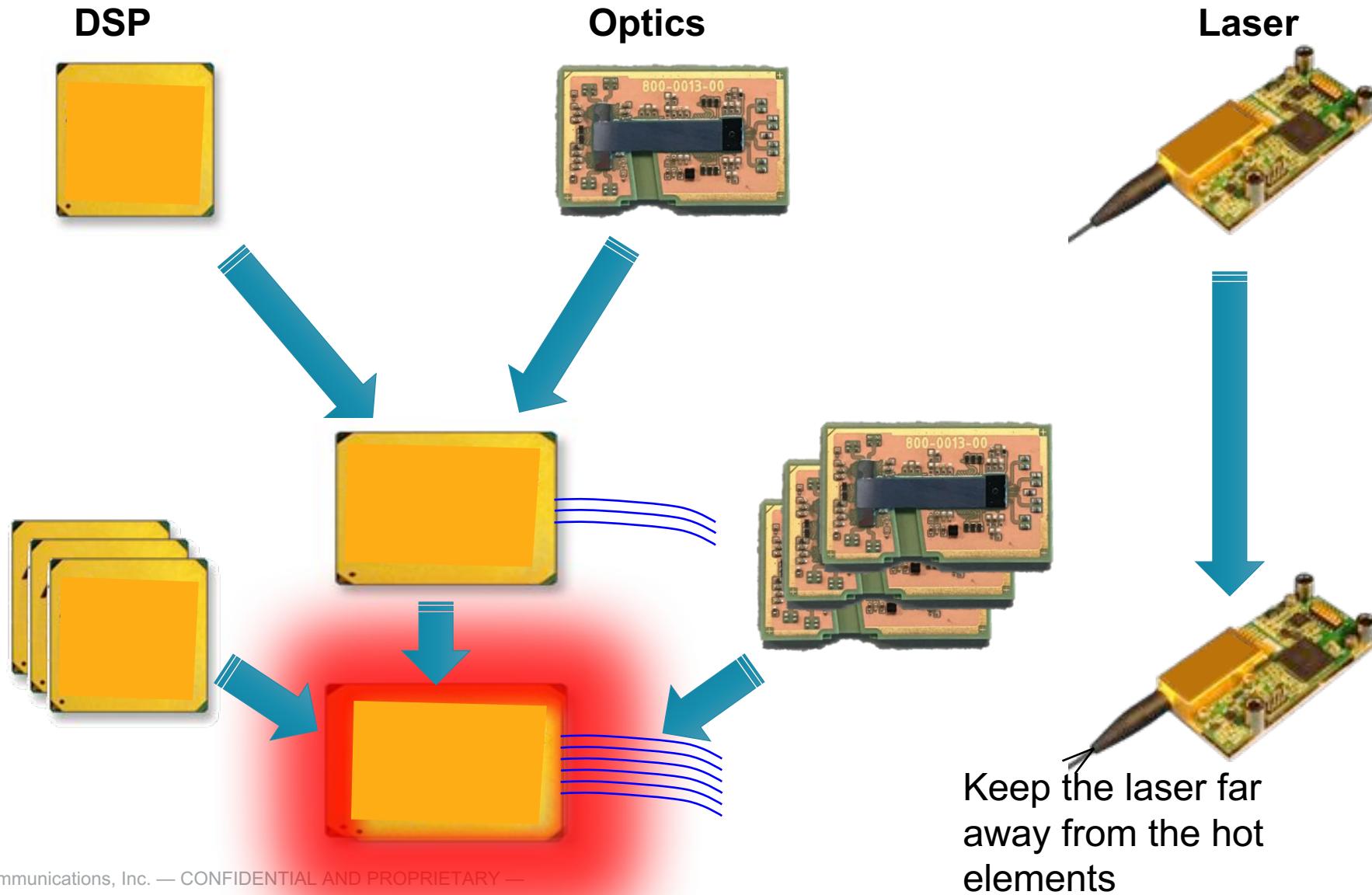


ASIC+PIC co-packaging

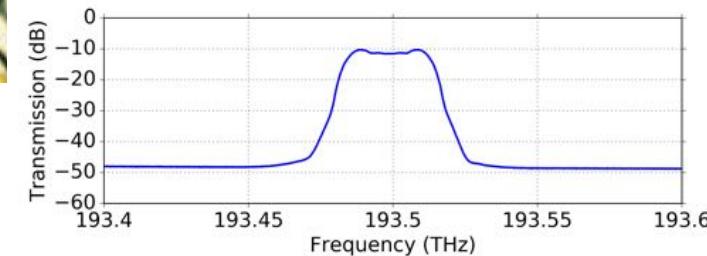
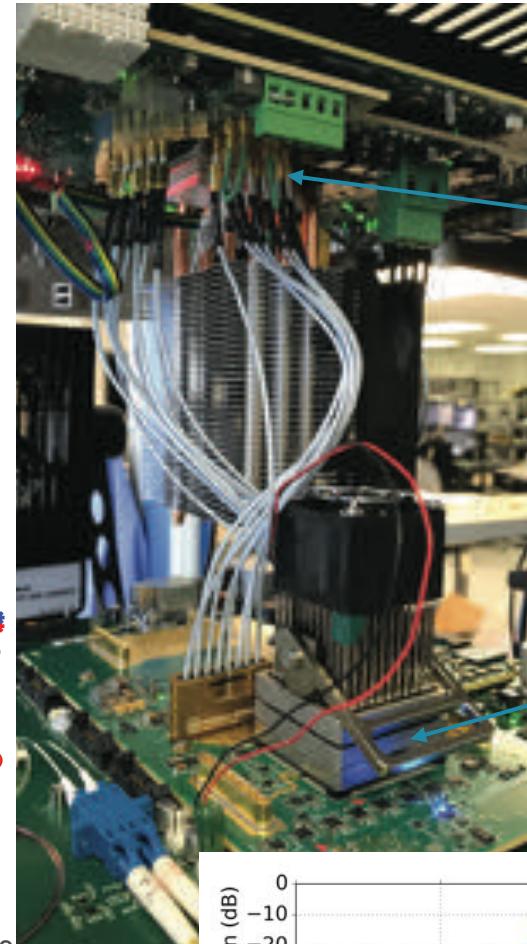
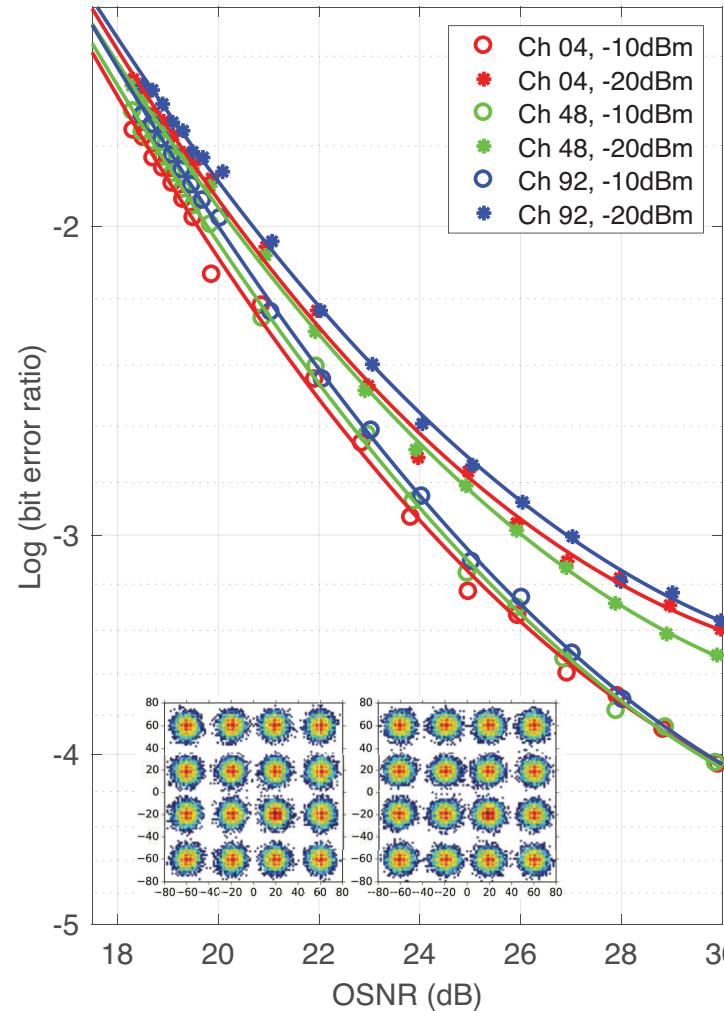
- Very high bandwidth connections
 - High speed analog signals never leave the package
- Smaller footprint
- Lower cost



Future evolution of coherent transceivers



240-Gb/s BGA testing

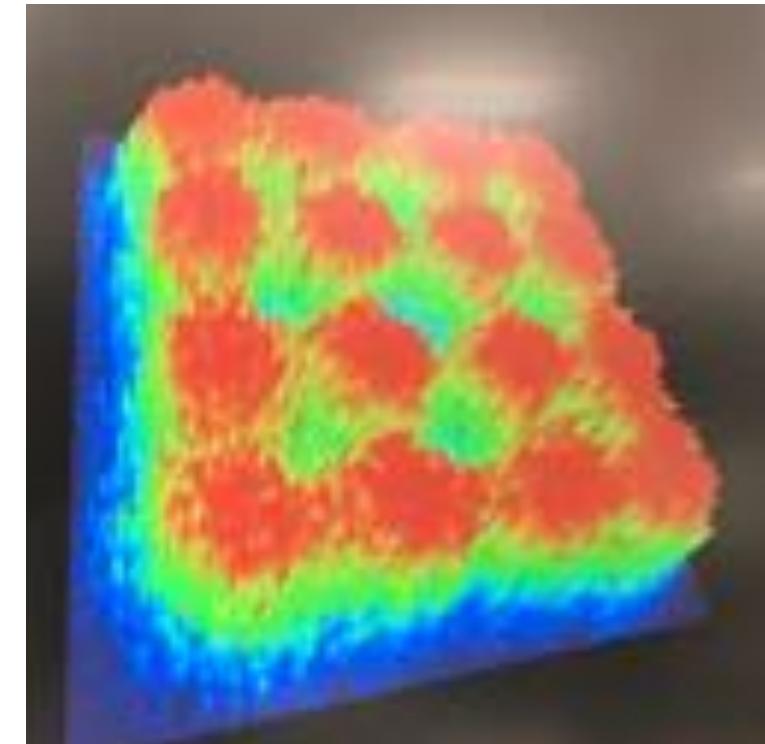


64-Gbaud testing



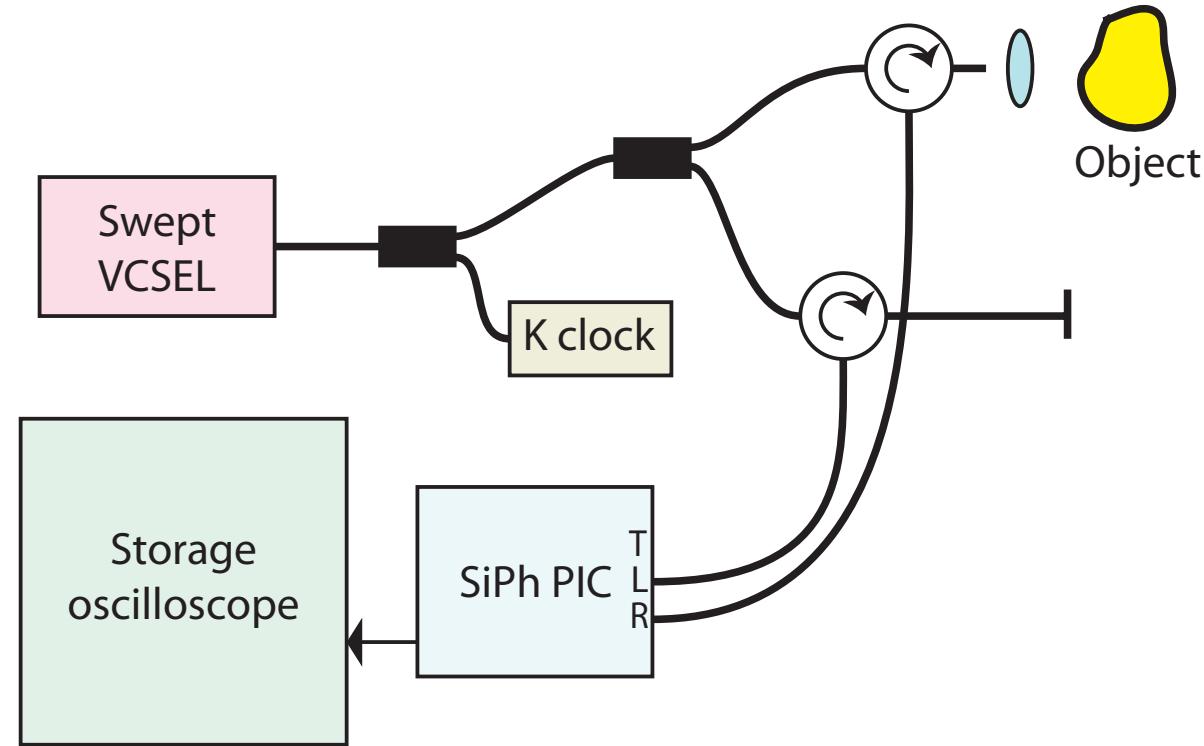
BGA PIC SMT on
PCB

16 QAM, single-pol 200-Gb/s



Imaging applications using SiPh coherent technology

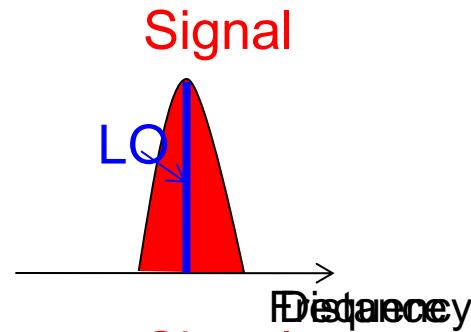
Optical coherence tomography



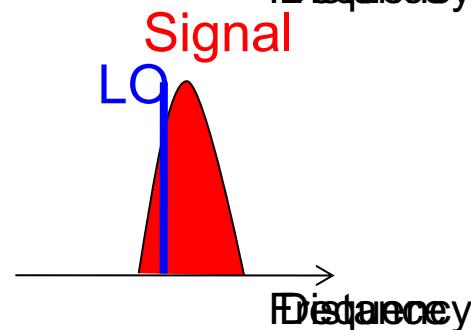
In collaboration with MIT and ThorLabs

Types of coherent detection

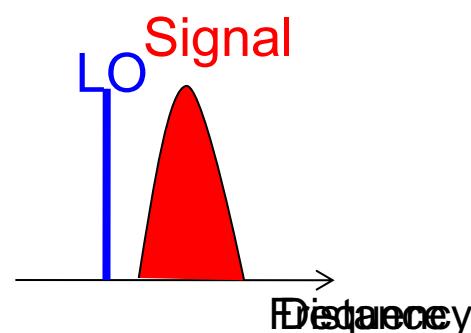
Homodyne



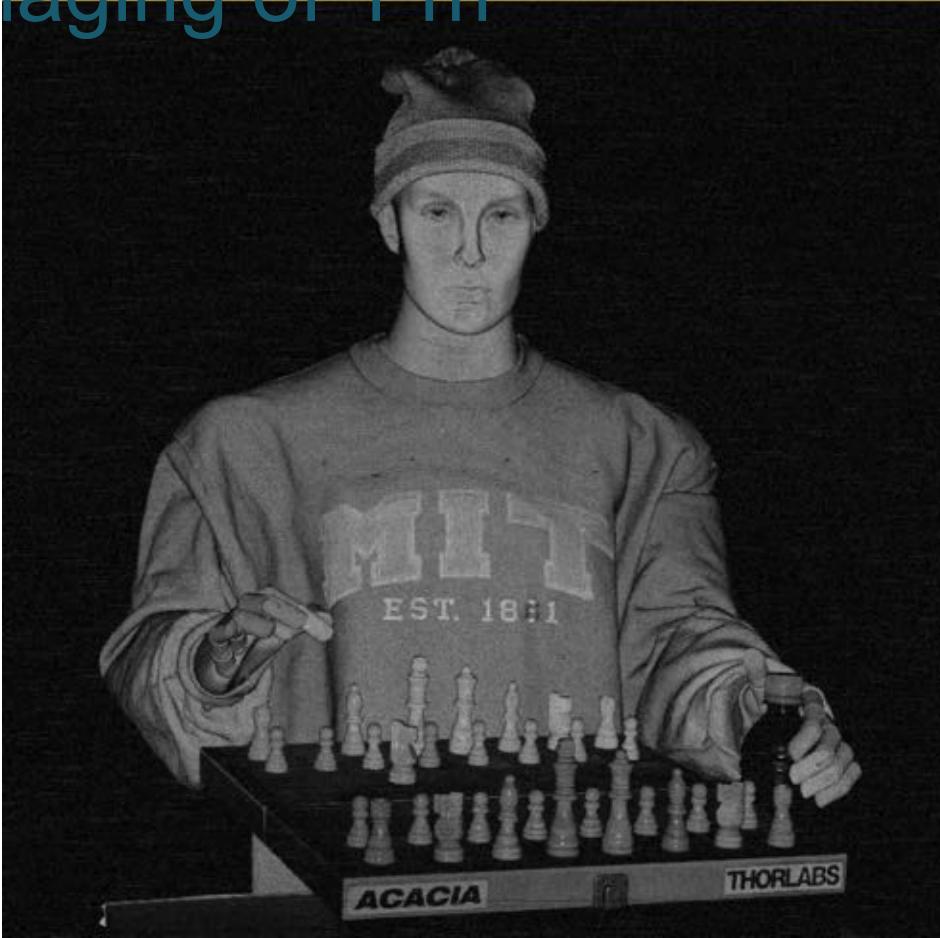
Intradyne



Heterodyne

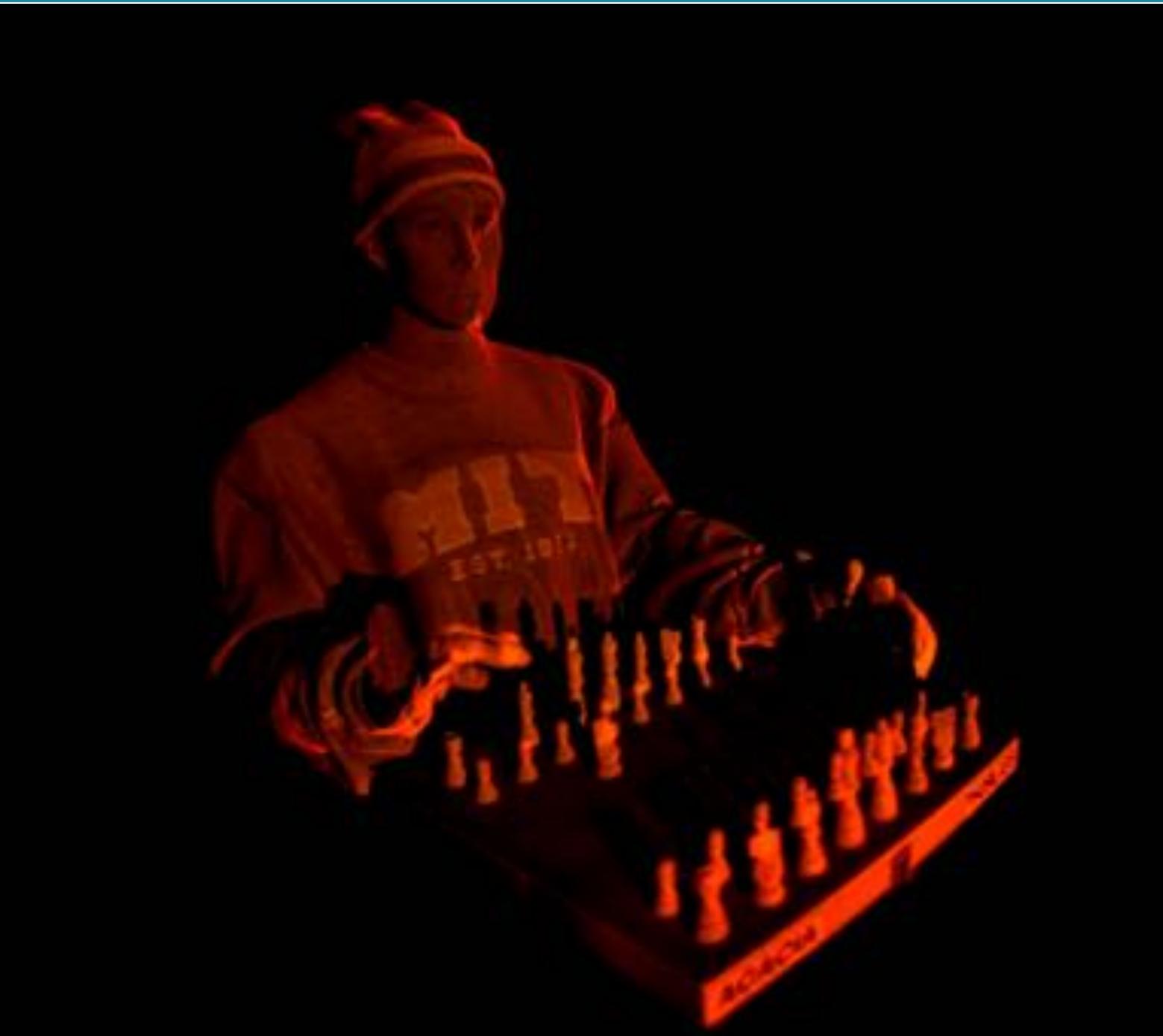


OCT imaging of 1 m³



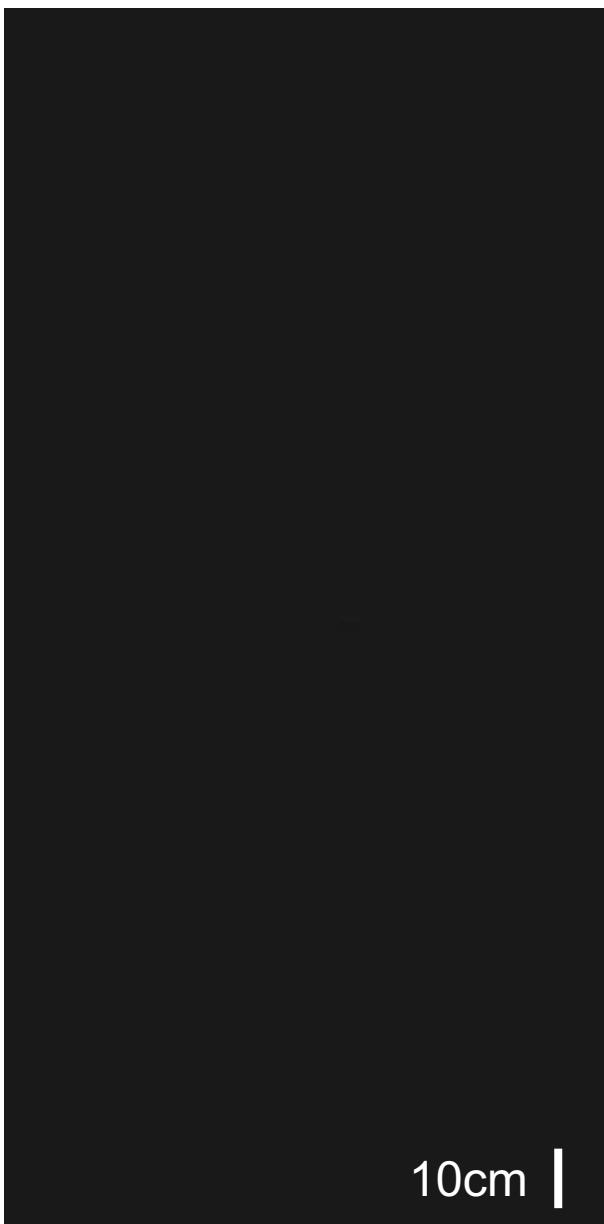
50cm |

- Scan pattern: 1000x1000 A-scans/volume
- Scan volume (~200cm depth, ~100cm horizontal, ~100cm vertical)
- Edge of chess board to back of mannequin ~80cm
- 0.4TB/volume, 200,000 points/A-line



Meter range OCT for 3D documentation

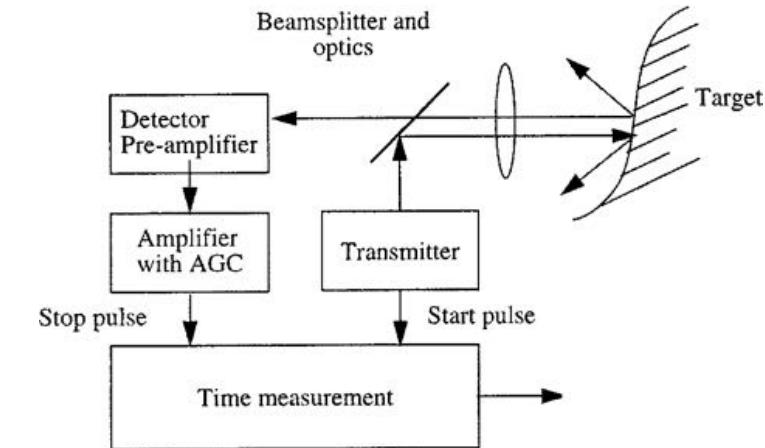




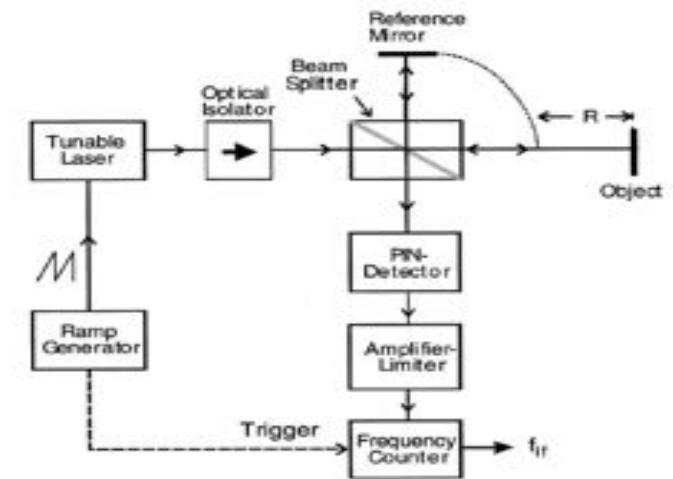


LiDAR

- Pulsed time-of-flight (TOF)
 - Simple
 - All today's LiDAR products employ TOF
 - Requires APDs
 - Most use 905 nm (1550nm is eye safe)

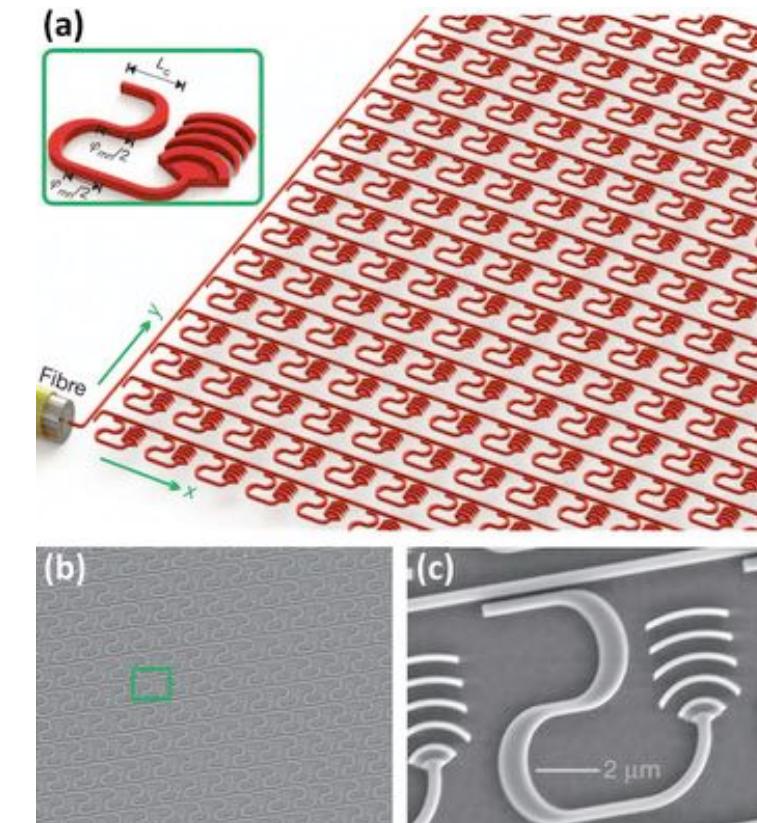
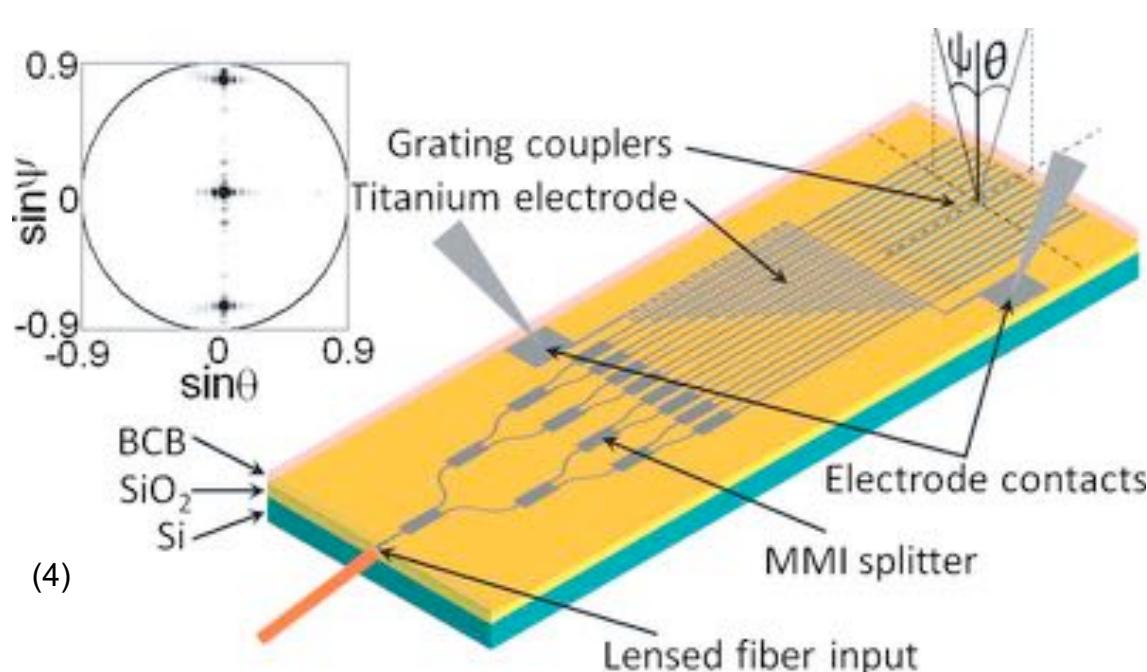


- Frequency modulated continuous wave (FMCW) (i.e., **coherent**)
 - More sensitive
 - Can use regular photodiodes
 - Gives more information (phase, Doppler shift)



Ref: Amann, Markus-Christian "Laser ranging: a ctrl review of usual techniques for distance measurement." Optical Eng 40.1 (2001): 10-19.

Phased-array beam steering using silicon photonics



K Van Acoleyen, et al., Opt. Lett, 2009.

J. Sun, et al., Adv. Photon. for Comm., 2014.

Conclusion

Conclusion

- SiPh allows for very high complexity with high yield and low-cost packaging
- Coherent optics is a killer application for SiPh

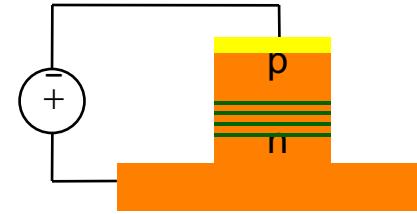
Thank you

Acknowledgments: **B. Mikkelsen**, E. Swanson, M. Givhechi, C. Rasmussen, **L. Chen**, R. Aroca, S. Azemati, J. Heanue, G. Ali, G. McBrien, Li Chen, **B. Guan**, H. Zhang, X. Zhang, **T. Nielsen**, H. Mezghani, M. Mihnev, **N. Sauer**, C. Yung, M. Xu, J. Fujimoto, B.

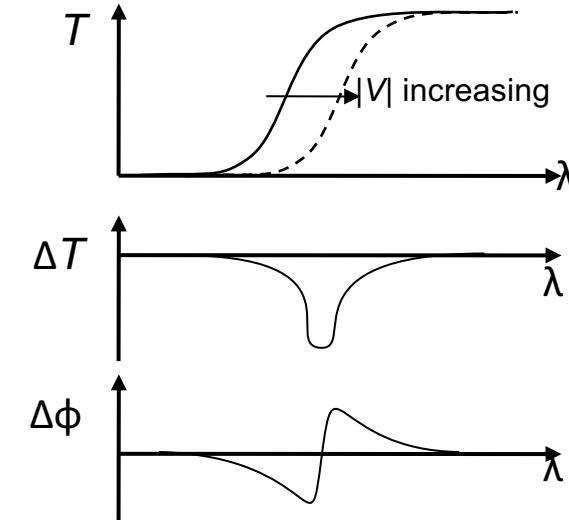
Back-up

InP & SiPh modulator comparison

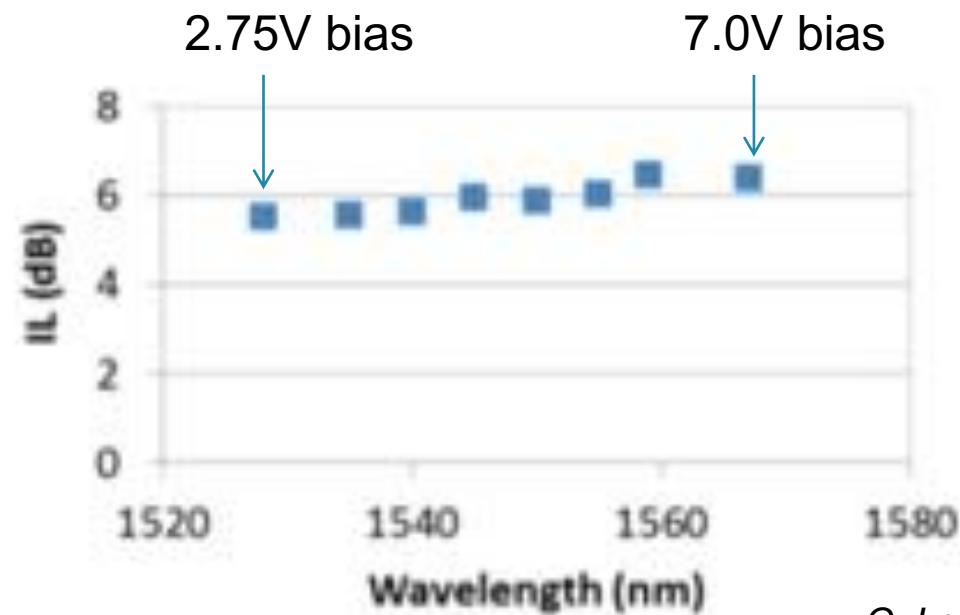
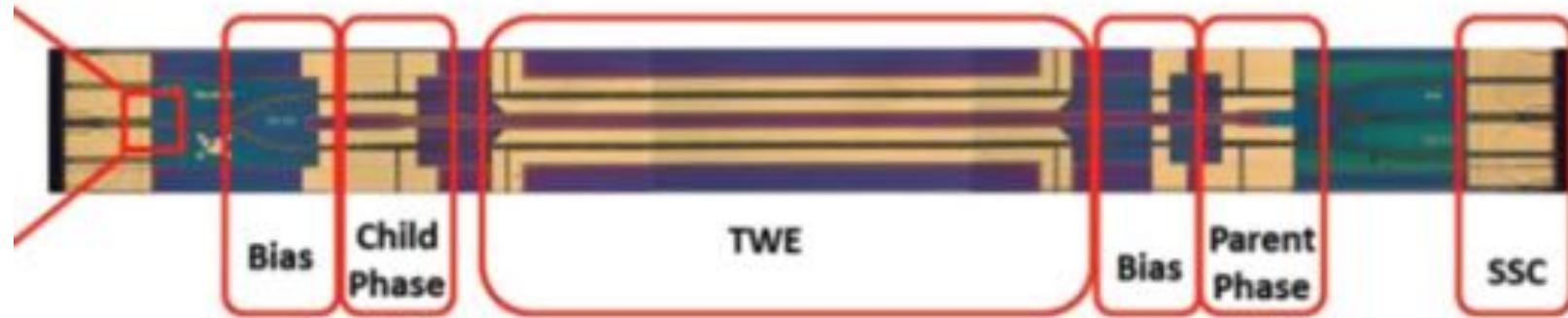
InP



$$\pi = 1 \text{ V-cm}$$



InP IQ modulator

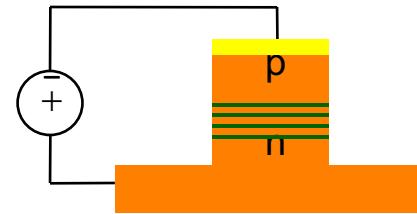


InP modulator bandwidth limited to ~40 nm

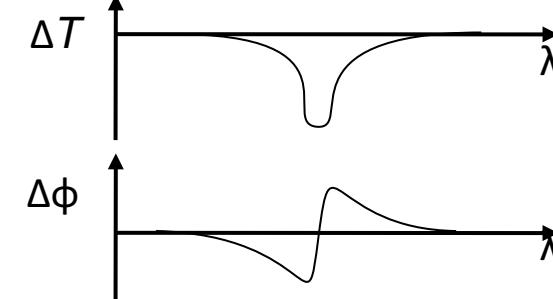
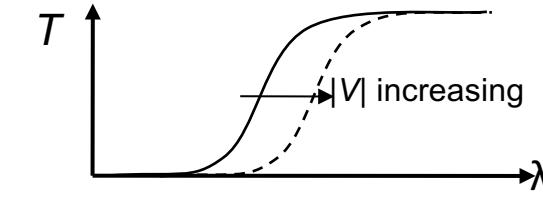
G. Letal, et al., OFC, Th4E.3, 2015.

InP & SiPh modulator comparison

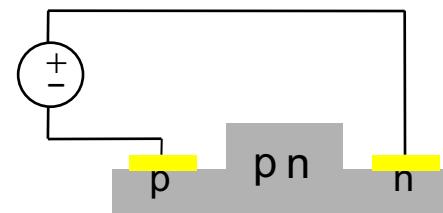
InP



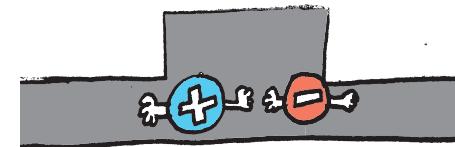
$$\pi = 1 \text{ V-cm}$$



Si



$$\pi = 2 \text{ V-cm}$$



$$\Delta n_r = -8.8 \times 10^{-22} N_e - 8.5 \times 10^{-18} N_h^{0.8}$$

$$\Delta n_i = 1.0 \times 10^{-22} N_e + 7.4 \times 10^{-23} N_h$$

N_e = free electron density
 N_h = free hole density